

### FITTING LOSS COEFFICIENTS

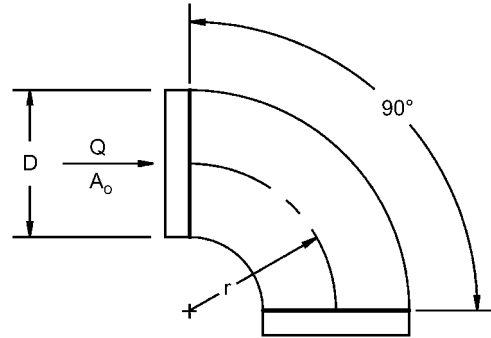
Fittings to support Examples 6 and 7 and some of the more common fittings are reprinted here.

For the complete fitting database see the *ASHRAE Duct Fitting Database (ASHRAE 2009)*.

#### ROUND FITTINGS

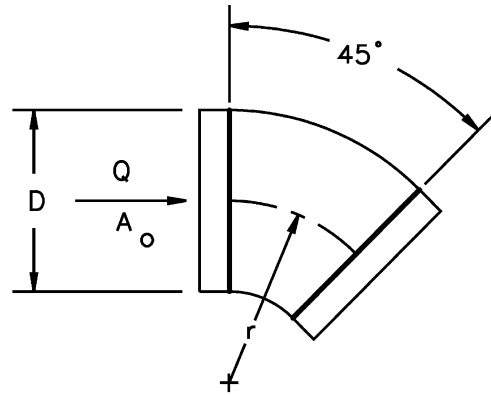
**CD3-1 Elbow, Die Stamped, 90 Degree,  $r/D = 1.5$**

$D, \text{mm}$	75	100	125	150	180	200	230	250
$C_o$	0.30	0.21	0.16	0.14	0.12	0.11	0.11	0.11



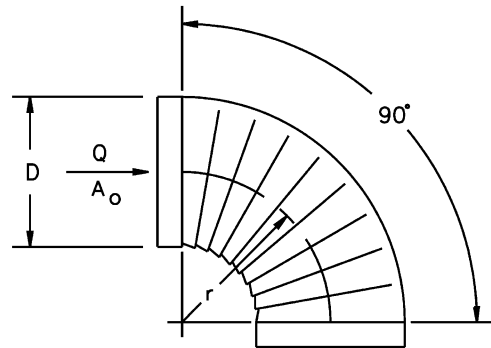
**CD3-3 Elbow, Die Stamped, 45 Degree,  $r/D = 1.5$**

$D, \text{mm}$	75	100	125	150	180	200	230	250
$C_o$	0.18	0.13	0.10	0.08	0.07	0.07	0.07	0.07



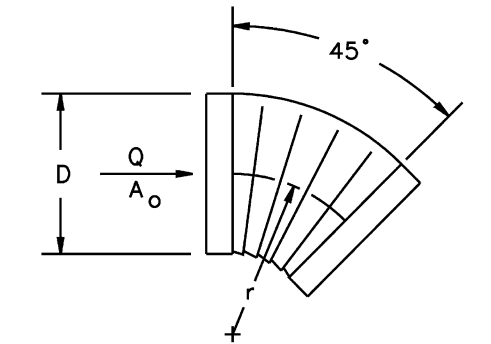
**CD3-5 Elbow, Pleated, 90 Degree,  $r/D = 1.5$**

$D, \text{mm}$	100	150	200	250	300	350	400
$C_o$	0.57	0.43	0.34	0.28	0.26	0.25	0.25



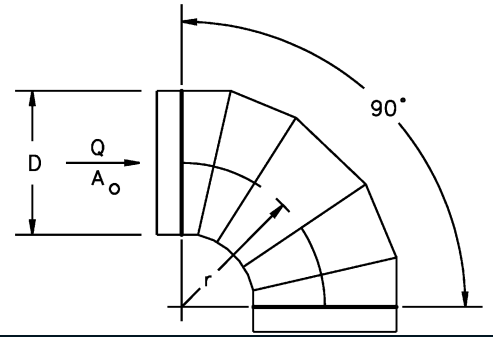
**CD3-7 Elbow, Pleated, 45 Degree,  $r/D = 1.5$**

$D, \text{mm}$	100	150	200	250	300	350	400
$C_o$	0.34	0.26	0.21	0.17	0.16	0.15	0.15



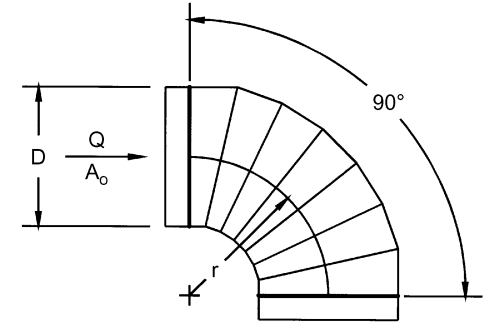
**CD3-9 Elbow, 5 Gore, 90 Degree,  $r/D = 1.5$**

$D, \text{mm}$	75	150	230	300	380	450	530	600	690	750	1500
$C_o$	0.51	0.28	0.21	0.18	0.16	0.15	0.14	0.13	0.12	0.12	0.12



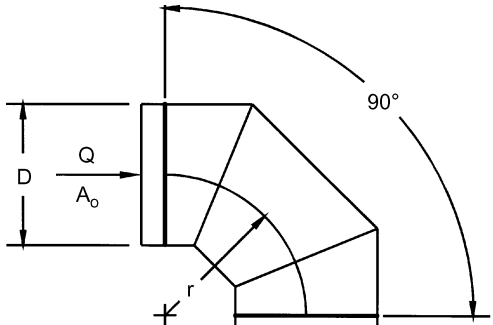
**CD3-10 Elbow, 7 Gore, 90 Degree,  $r/D = 2.5$**

$D, \text{mm}$	75	150	230	300	380	450	690	1500
$C_o$	0.16	0.12	0.10	0.08	0.07	0.06	0.05	0.03



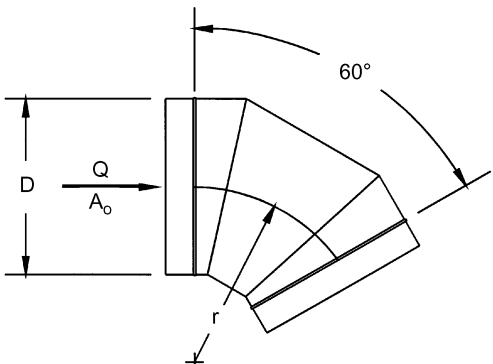
**CD3-12 Elbow, 3 Gore, 90 Degree,  $r/D = 0.75$  to  $2.0$**

$r/D$	0.75	1.00	1.50	2.00
$C_o$	0.54	0.42	0.34	0.33



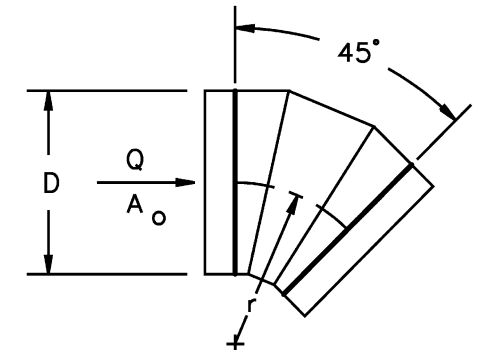
**CD3-13 Elbow, 3 Gore, 60 Degree,  $r/D = 1.5$**

$D, \text{mm}$	75	150	230	300	380	450	530	600	690	750	1500
$C_o$	0.40	0.21	0.16	0.14	0.12	0.12	0.11	0.10	0.09	0.09	0.09



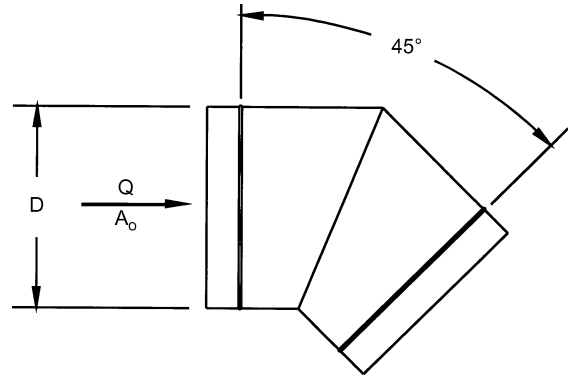
**CD3-14 Elbow, 3 Gore, 45 Degree,  $r/D = 1.5$**

$D, \text{mm}$	75	150	230	300	380	450	530	600	690	750	1500
$C_o$	0.31	0.17	0.13	0.11	0.11	0.09	0.08	0.08	0.07	0.07	0.07



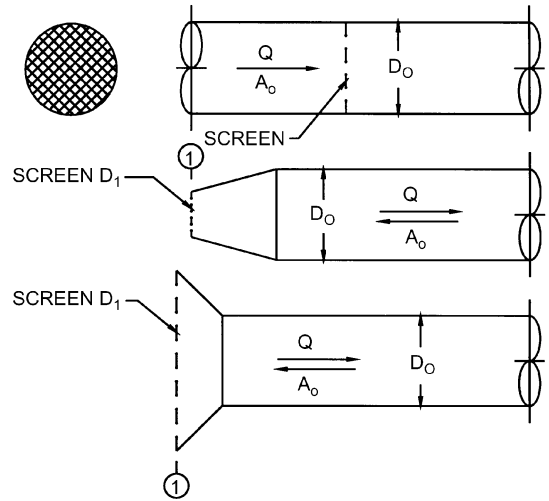
**CD3-17 Elbow, Mitered, 45 Degree**

D, mm	75	150	230	300	380	450	530	600	690	1500
$C_o$	0.87	0.79	0.74	0.72	0.71	0.70	0.69	0.68	0.68	0.67



**CD6-1 Screen (Only)**

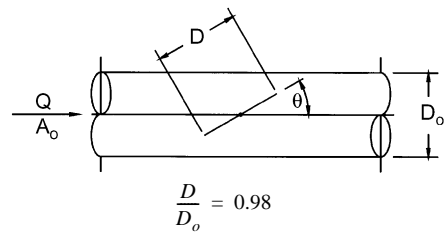
$A_1/A_o$	$C_o$ Values													
	$n$													
0.2	155.00	102.50	75.00	55.00	41.25	31.50	24.25	18.75	14.50	11.00	8.00	3.50	0.0	0.0
0.3	68.89	45.56	33.33	24.44	18.33	14.00	10.78	8.33	6.44	4.89	3.56	1.56	0.0	0.0
0.4	38.75	25.63	18.75	13.75	10.31	7.88	6.06	4.69	3.63	2.75	2.00	0.88	0.0	0.0
0.5	24.80	16.40	12.00	8.80	6.60	5.04	3.88	3.00	2.32	1.76	1.28	0.56	0.0	0.0
0.6	17.22	11.39	8.33	6.11	4.58	3.50	2.69	2.08	1.61	1.22	0.89	0.39	0.0	0.0
0.7	12.65	8.37	6.12	4.49	3.37	2.57	1.98	1.53	1.18	0.90	0.65	0.29	0.0	0.0
0.8	9.69	6.40	4.69	3.44	2.58	1.97	1.52	1.17	0.91	0.69	0.50	0.22	0.0	0.0
0.9	7.65	5.06	3.70	2.72	2.04	1.56	1.20	0.93	0.72	0.54	0.40	0.17	0.0	0.0
1.0	6.20	4.10	3.00	2.20	1.65	1.26	0.97	0.75	0.58	0.44	0.32	0.14	0.0	0.0
1.2	4.31	2.85	2.08	1.53	1.15	0.88	0.67	0.52	0.40	0.31	0.22	0.10	0.0	0.0
1.4	3.16	2.09	1.53	1.12	0.84	0.64	0.49	0.38	0.30	0.22	0.16	0.07	0.0	0.0
1.6	2.42	1.60	1.17	0.86	0.64	0.49	0.38	0.29	0.23	0.17	0.13	0.05	0.0	0.0
1.8	1.91	1.27	0.93	0.68	0.51	0.39	0.30	0.23	0.18	0.14	0.10	0.04	0.0	0.0
2.0	1.55	1.03	0.75	0.55	0.41	0.32	0.24	0.19	0.15	0.11	0.08	0.04	0.0	0.0
2.5	0.99	0.66	0.48	0.35	0.26	0.20	0.16	0.12	0.09	0.07	0.05	0.02	0.0	0.0
3.0	0.69	0.46	0.33	0.24	0.18	0.14	0.11	0.08	0.06	0.05	0.04	0.02	0.0	0.0
4.0	0.39	0.26	0.19	0.14	0.10	0.08	0.06	0.05	0.04	0.03	0.02	0.01	0.0	0.0
6.0	0.17	0.11	0.08	0.06	0.05	0.04	0.03	0.02	0.02	0.01	0.01	0.00	0.0	0.0



$n$  = free area ratio of screen  
 $A_o$  = area of duct  
 $A_1$  = cross-sectional area of duct or fitting where screen is located

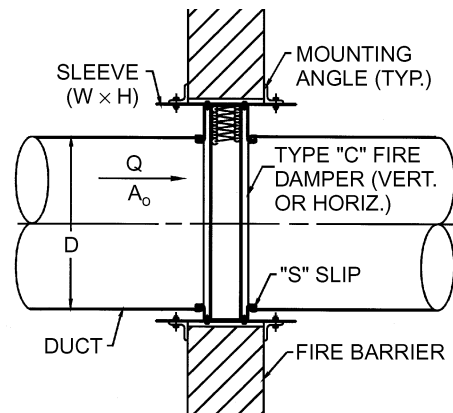
**CD9-1 Damper, Butterfly**

$\theta$	0	10	20	30	40	50	60	70	75	90
$C_o$	0.60	0.85	1.70	4.0	9.4	24	67	215	400	9999



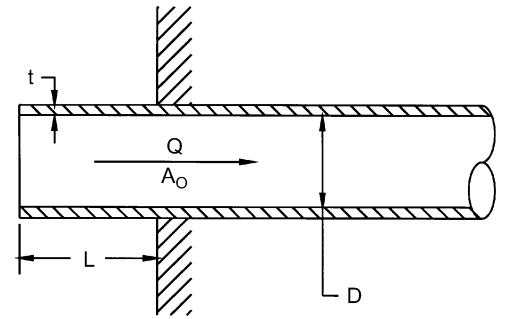
**CD9-3 Fire Damper, Curtain Type, Type C, Horizontal Duct**

$C_o = 0.12$



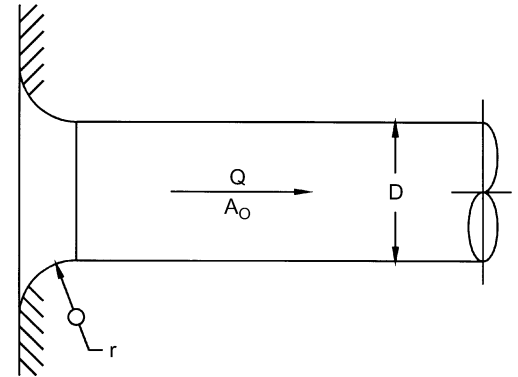
**ED1-1 Duct Mounted in Wall**

$t/D$	$C_o$ Values								
	$L/D$								
	0.0	0.002	0.01	0.05	0.10	0.20	0.30	0.50	10.0
0.00	0.50	0.57	0.68	0.80	0.86	0.92	0.97	1.00	1.00
0.02	0.50	0.51	0.52	0.55	0.60	0.66	0.69	0.72	0.72
0.05	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
10.00	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50



**ED1-3 Bellmouth, with Wall**

$r/D$	0.0	0.01	0.02	0.03	0.04	0.05	0.06	0.08	0.10	0.12	0.16	0.20	10.0
$C_o$	0.50	0.44	0.37	0.31	0.26	0.22	0.20	0.15	0.12	0.09	0.06	0.03	0.03

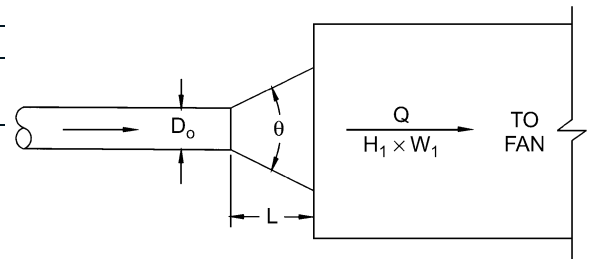


**ED2-1 Conical Diffuser, Round to Plenum, Exhaust/Return Systems**

$A_1/A_o$	$C_o$ Values												
	$L/D_o$												
	0.5	1.0	2.0	3.0	4.0	5.0	6.0	8.0	10.0	12.0	14.0		
1.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
1.5	0.03	0.02	0.03	0.03	0.04	0.05	0.06	0.08	0.10	0.11	0.13		
2.0	0.08	0.06	0.04	0.04	0.04	0.05	0.05	0.06	0.08	0.09	0.10		
2.5	0.13	0.09	0.06	0.06	0.06	0.06	0.06	0.06	0.07	0.08	0.09		
3.0	0.17	0.12	0.09	0.07	0.07	0.06	0.06	0.07	0.07	0.08	0.08		
4.0	0.23	0.17	0.12	0.10	0.09	0.08	0.08	0.08	0.08	0.08	0.08		
6.0	0.30	0.22	0.16	0.13	0.12	0.10	0.10	0.09	0.09	0.09	0.08		
8.0	0.34	0.26	0.18	0.15	0.13	0.12	0.11	0.10	0.09	0.09	0.09		
10.0	0.36	0.28	0.20	0.16	0.14	0.13	0.12	0.11	0.10	0.09	0.09		
14.0	0.39	0.30	0.22	0.18	0.16	0.14	0.13	0.12	0.10	0.10	0.10		
20.0	0.41	0.32	0.24	0.20	0.17	0.15	0.14	0.12	0.11	0.11	0.10		
1000.0	0.41	0.32	0.24	0.20	0.17	0.15	0.14	0.12	0.11	0.11	0.10		

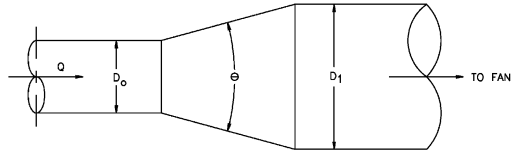
  

$A_1/A_o$	Optimum Angle $\theta$ , degrees										
	0.5	1.0	2.0	3.0	4.0	5.0	6.0	8.0	10.0	12.0	14.0
1.0	0	0	0	0	0	0	0	0	0	0	0
1.5	17	10	6.5	4.5	3.5	2.8	2.2	1.7	1.2	1.0	0.8
2.0	21	14	8.5	6.2	5.0	4.3	3.8	3.0	2.3	2.0	1.6
2.5	25	16	10	7.4	6.0	5.4	4.8	4.0	3.5	3.0	2.5
3.0	27	17	11	8.5	7.0	6.1	5.6	4.8	4.2	3.8	3.2
4.0	29	20	13	9.8	8.0	7.2	6.6	5.8	5.2	4.8	4.4
6.0	31	21	14	11	9.4	8.2	7.4	6.2	5.6	5.2	4.7
8.0	32	22	15	12	10	8.8	8.0	6.6	5.8	5.4	5.0
33	33	23	15	12	11	9.4	8.4	7.0	6.2	5.5	5.2
14.0	33	24	16	13	11	9.6	8.7	7.3	6.3	5.6	5.4
20.0	34	24	16	13	11	9.8	9.0	7.5	6.5	6.0	5.6
1000.0	34	24	16	13	11	9.8	9.0	7.5	6.5	6.0	5.6



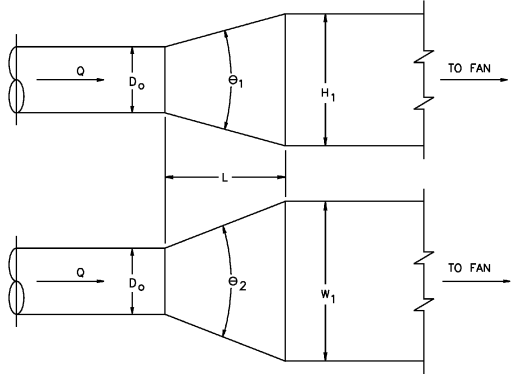
**ED4-1 Transition, Round to Round, Exhaust/Return Systems**

$A_o/A_1$	$C_o$ Values												
	$\theta$												
	0	3	5	10	15	20	30	45	60	90	120	150	180
0.063	0.0	0.18	0.18	0.20	0.29	0.38	0.60	0.84	0.88	0.88	0.88	0.88	0.88
0.10	0.0	0.20	0.18	0.20	0.27	0.38	0.59	0.76	0.80	0.83	0.84	0.83	0.83
0.167	0.0	0.18	0.17	0.18	0.25	0.33	0.48	0.66	0.77	0.74	0.73	0.73	0.72
0.25	0.0	0.20	0.17	0.16	0.21	0.30	0.46	0.61	0.68	0.64	0.63	0.62	0.62
0.50	0.0	0.15	0.13	0.11	0.13	0.19	0.32	0.33	0.33	0.32	0.31	0.30	0.30
1.00	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.00	0.0	0.30	0.26	0.21	0.19	0.19	0.19	0.23	0.27	0.51	0.73	0.90	0.95
4.00	0.0	1.60	1.14	0.75	0.70	0.70	0.70	0.90	1.09	2.78	4.29	5.63	6.53
6.00	0.0	3.89	3.02	1.73	1.58	1.58	1.58	2.12	2.66	6.62	10.01	13.03	15.12
10.00	0.0	11.80	9.30	5.30	5.00	5.00	5.00	6.45	7.90	19.00	28.50	36.70	42.70

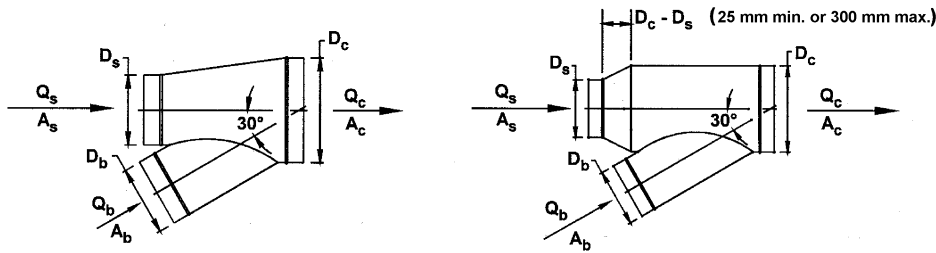


**ED4-2 Transition, Round to Rectangular, Exhaust/Return Systems**

$A_o/A_1$	$C_o$ Values												
	$\theta$												
	0	3	5	10	15	20	30	45	60	90	120	150	180
0.063	0.0	0.17	0.19	0.30	0.46	0.53	0.64	0.77	0.88	0.95	0.95	0.94	0.93
0.10	0.0	0.17	0.19	0.30	0.45	0.53	0.64	0.75	0.84	0.89	0.89	0.89	0.88
0.167	0.0	0.18	0.19	0.30	0.44	0.53	0.63	0.72	0.78	0.79	0.79	0.79	0.79
0.25	0.0	0.16	0.18	0.25	0.36	0.45	0.52	0.58	0.62	0.64	0.64	0.64	0.64
0.50	0.0	0.14	0.14	0.15	0.22	0.25	0.30	0.33	0.33	0.33	0.32	0.31	0.30
1.00	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.00	0.0	0.30	0.27	0.26	0.28	0.25	0.19	0.23	0.27	0.52	0.75	0.91	0.95
4.00	0.0	1.60	1.14	0.84	0.85	0.86	0.76	0.90	1.09	2.78	4.30	5.65	6.55
6.00	0.0	3.89	3.04	1.84	1.77	1.78	1.73	2.18	2.67	6.67	10.07	13.09	15.18
10.00	0.0	11.80	9.31	5.40	5.18	5.15	5.05	6.44	7.94	19.06	28.55	36.75	42.75



**ED5-1 Wye, 30 Degree, Converging**



		$C_b$ Values								
		$Q_b/Q_c$								
$A_s/A_c$	$A_b/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1	0.1	-13.25	-1.80	0.01	0.55	0.75	0.84	0.88	0.91	0.97
	0.2	-56.10	-10.12	-2.80	-0.63	0.19	0.53	0.69	0.75	0.78
	0.3	-127.28	-23.81	-7.31	-2.44	-0.59	0.19	0.52	0.66	0.70
	0.4	-226.84	-42.88	-13.55	-4.89	-1.61	-0.22	0.38	0.62	0.68
	0.5	-354.79	-67.34	-21.52	-7.98	-2.86	-0.69	0.24	0.61	0.70
	0.6	-511.13	-97.21	-31.22	-11.73	-4.35	-1.23	0.11	0.64	0.77
	0.7	-695.87	-132.47	-42.66	-16.13	-6.08	-1.84	0.00	0.71	0.89
	0.8	-909.01	-173.14	-55.83	-21.17	-8.05	-2.51	-0.12	0.82	1.05
	0.9	-1151.	-219.20	-70.73	-26.87	-10.27	-3.25	-0.22	0.97	1.26
	1.0	-1420.	-270.66	-87.36	-33.21	-12.72	-4.05	-0.31	1.15	1.51

ED5-1 Wye, 30 Degree, Converging (Continued)

		<i>C<sub>b</sub> Values (Continued)</i>								
		<i>Q<sub>b</sub>/Q<sub>c</sub></i>								
<i>A<sub>s</sub>/A<sub>c</sub></i>	<i>A<sub>p</sub>/A<sub>c</sub></i>	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.2	0.1	-5.30	-0.24	0.54	0.77	0.85	0.88	0.90	0.93	0.98
	0.2	-24.17	-3.78	-0.60	0.30	0.64	0.77	0.83	0.88	0.98
	0.3	-55.88	-9.77	-2.57	-0.50	0.25	0.55	0.67	0.70	0.71
	0.4	-99.93	-17.94	-5.13	-1.45	-0.11	0.42	0.62	0.68	0.68
	0.5	-156.51	-28.40	-8.37	-2.62	-0.52	0.30	0.62	0.71	0.69
	0.6	-225.62	-41.13	-12.30	-4.01	-0.99	0.20	0.66	0.78	0.75
	0.7	-307.26	-56.14	-16.90	-5.61	-1.51	0.11	0.73	0.90	0.86
	0.8	-401.44	-73.44	-22.18	-7.44	-2.08	0.04	0.84	1.06	1.01
	0.9	-508.15	-93.02	-28.15	-9.49	-2.71	-0.03	0.99	1.27	1.20
	1.0	-627.39	-114.89	-34.80	-11.77	-3.39	-0.08	1.18	1.52	1.43
0.3	0.1	-2.77	0.26	0.71	0.83	0.88	0.90	0.91	0.93	0.99
	0.2	-13.97	-1.77	0.08	0.59	0.77	0.84	0.88	0.92	1.06
	0.3	-33.06	-5.33	-1.09	0.10	0.51	0.66	0.71	0.72	0.74
	0.4	-59.43	-10.08	-2.52	-0.41	0.32	0.59	0.67	0.68	0.66
	0.5	-93.24	-16.11	-4.30	-1.00	0.14	0.56	0.69	0.70	0.66
	0.6	-134.51	-23.45	-6.44	-1.68	-0.03	0.57	0.76	0.77	0.70
	0.7	-183.25	-32.08	-8.93	-2.45	-0.21	0.61	0.87	0.88	0.79
	0.8	-239.47	-42.01	-11.77	-3.32	-0.38	0.69	1.02	1.03	0.91
	0.9	-303.16	-53.25	-14.97	-4.27	-0.56	0.80	1.21	1.23	1.07
	1.0	-374.32	-65.79	-18.53	-5.32	-0.73	0.94	1.45	1.47	1.27
0.4	0.1	-1.58	0.48	0.78	0.86	0.89	0.90	0.91	0.93	0.99
	0.2	-9.20	-0.85	0.39	0.71	0.82	0.87	0.90	0.94	1.09
	0.3	-22.31	-3.24	-0.38	0.39	0.64	0.73	0.76	0.78	0.85
	0.4	-40.52	-6.48	-1.37	0.02	0.48	0.64	0.67	0.66	0.65
	0.5	-63.71	-10.50	-2.50	-0.33	0.40	0.63	0.69	0.67	0.63
	0.6	-92.00	-15.37	-3.84	-0.71	0.33	0.67	0.75	0.71	0.65
	0.7	-125.40	-21.08	-5.40	-1.13	0.28	0.75	0.85	0.80	0.70
	0.8	-163.90	-27.65	-7.16	-1.59	0.25	0.86	1.00	0.93	0.80
	0.9	-207.52	-35.07	-9.14	-2.09	0.25	1.02	1.18	1.10	0.93
	1.0	-256.25	-43.35	-11.33	-2.63	0.26	1.21	1.42	1.31	1.09
0.5	0.1	-0.94	0.60	0.82	0.87	0.89	0.90	0.91	0.93	0.99
	0.2	-6.62	-0.36	0.54	0.77	0.85	0.88	0.90	0.95	1.11
	0.3	-16.42	-2.11	-0.01	0.54	0.72	0.78	0.80	0.83	0.96
	0.4	-30.26	-4.59	-0.79	0.22	0.54	0.64	0.66	0.64	0.64
	0.5	-47.68	-7.55	-1.61	-0.02	0.48	0.63	0.65	0.62	0.59
	0.6	-68.93	-11.13	-2.56	-0.28	0.45	0.67	0.69	0.65	0.58
	0.7	-94.00	-15.31	-3.65	-0.55	0.44	0.74	0.77	0.71	0.61
	0.8	-122.90	-20.12	-4.88	-0.83	0.46	0.85	0.90	0.81	0.68
	0.9	-155.63	-25.54	-6.25	-1.12	0.51	1.00	1.06	0.94	0.77
	1.0	-192.18	-31.58	-7.77	-1.43	0.59	1.19	1.26	1.12	0.90
0.6	0.1	-0.57	0.66	0.84	0.88	0.89	0.90	0.91	0.93	0.99
	0.2	-5.12	-0.10	0.62	0.79	0.85	0.87	0.90	0.95	1.11
	0.3	-13.00	-1.49	0.18	0.61	0.75	0.79	0.82	0.86	1.02
	0.4	-24.31	-3.55	-0.50	0.30	0.55	0.62	0.63	0.62	0.63
	0.5	-38.41	-5.94	-1.16	0.09	0.48	0.59	0.60	0.57	0.55
	0.6	-55.58	-8.80	-1.92	-0.12	0.45	0.61	0.62	0.57	0.52
	0.7	-75.83	-12.16	-2.79	-0.33	0.44	0.66	0.67	0.60	0.52
	0.8	-99.17	-16.00	-3.76	-0.54	0.46	0.74	0.76	0.67	0.56
	0.9	-125.60	-20.33	-4.83	-0.76	0.51	0.86	0.88	0.77	0.62
	1.0	-155.12	-25.14	-6.02	-0.99	0.58	1.02	1.04	0.90	0.71
0.7	0.1	-0.35	0.70	0.84	0.88	0.89	0.90	0.90	0.92	0.99
	0.2	-4.24	0.05	0.65	0.80	0.85	0.87	0.89	0.94	1.12
	0.3	-11.00	-1.15	0.27	0.63	0.75	0.79	0.82	0.87	1.06
	0.4	-20.82	-3.00	-0.38	0.31	0.52	0.59	0.60	0.59	0.61
	0.5	-32.99	-5.09	-0.98	0.10	0.43	0.53	0.54	0.52	0.51
	0.6	-47.78	-7.58	-1.67	-0.11	0.38	0.52	0.53	0.49	0.45
	0.7	-65.22	-10.50	-2.44	-0.32	0.34	0.53	0.54	0.49	0.43
	0.8	-85.32	-13.83	-3.30	-0.53	0.33	0.58	0.59	0.52	0.43
	0.9	-108.07	-17.58	-4.26	-0.75	0.34	0.66	0.67	0.58	0.46
	1.0	-133.48	-21.76	-5.30	-0.97	0.38	0.76	0.78	0.67	0.51
0.8	0.1	-0.23	0.71	0.84	0.88	0.89	0.89	0.90	0.92	0.98
	0.2	-3.75	0.11	0.65	0.79	0.84	0.86	0.88	0.94	1.12
	0.3	-9.88	-0.99	0.29	0.63	0.74	0.78	0.81	0.87	1.09
	0.4	-18.88	-2.75	-0.36	0.28	0.48	0.55	0.56	0.57	0.61
	0.5	-29.98	-4.71	-0.96	0.04	0.36	0.46	0.47	0.46	0.47
	0.6	-43.46	-7.05	-1.64	-0.20	0.26	0.41	0.43	0.41	0.39
	0.7	-59.34	-9.77	-2.40	-0.44	0.19	0.38	0.41	0.38	0.34
	0.8	-77.64	-12.88	-3.26	-0.69	0.13	0.38	0.42	0.37	0.31
	0.9	-98.35	-16.38	-4.20	-0.95	0.09	0.40	0.45	0.39	0.30
	1.0	-121.48	-20.27	-5.24	-1.23	0.06	0.45	0.51	0.43	0.31

## ED5-1 Wye, 30 Degree, Converging (Continued)

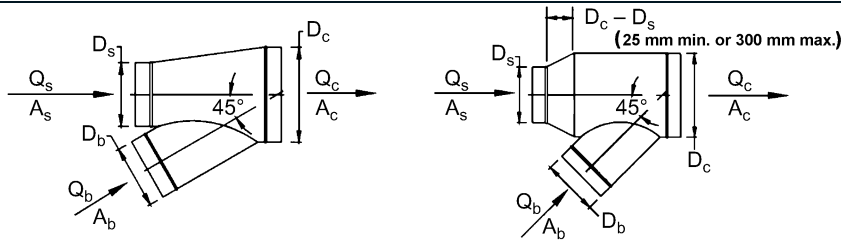
		<i>C<sub>b</sub> Values (Concluded)</i>								
<i>A<sub>s</sub>/A<sub>c</sub></i>	<i>A<sub>b</sub>/A<sub>c</sub></i>	<i>Q<sub>b</sub>/Q<sub>c</sub></i>								
		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.9	0.1	-0.18	0.72	0.84	0.87	0.88	0.89	0.90	0.92	0.98
	0.2	-3.52	0.12	0.64	0.78	0.82	0.85	0.88	0.93	1.12
	0.3	-9.34	-0.95	0.28	0.60	0.71	0.76	0.80	0.87	1.10
	0.4	-17.96	-2.70	-0.40	0.22	0.43	0.50	0.53	0.54	0.60
	0.5	-28.58	-4.65	-1.05	-0.07	0.26	0.37	0.40	0.41	0.42
	0.6	-41.45	-6.97	-1.77	-0.35	0.12	0.28	0.32	0.32	0.32
	0.7	-56.61	-9.66	-2.58	-0.65	0.00	0.21	0.27	0.26	0.24
	0.8	-74.08	-12.74	-3.49	-0.97	-0.12	0.16	0.23	0.22	0.18
	0.9	-93.84	-16.21	-4.50	-1.30	-0.23	0.13	0.21	0.19	0.14
	1.0	-115.92	-20.06	-5.61	-1.66	-0.34	0.11	0.21	0.18	0.11
1.0	0.1	-0.17	0.71	0.83	0.87	0.88	0.89	0.90	0.92	0.98
	0.2	-3.48	0.10	0.62	0.76	0.81	0.84	0.87	0.92	1.11
	0.3	-9.22	-1.00	0.23	0.56	0.68	0.74	0.78	0.86	1.11
	0.4	-17.76	-2.79	-0.50	0.14	0.37	0.45	0.49	0.52	0.60
	0.5	-28.31	-4.82	-1.21	-0.20	0.15	0.28	0.33	0.35	0.38
	0.6	-41.06	-7.21	-2.01	-0.55	-0.04	0.15	0.22	0.23	0.25
	0.7	-56.09	-9.99	-2.91	-0.92	-0.23	0.03	0.12	0.14	0.15
	0.8	-73.39	-13.17	-3.92	-1.32	-0.41	-0.07	0.04	0.06	0.06
	0.9	-92.98	-16.75	-5.04	-1.75	-0.60	-0.17	-0.03	-0.01	-0.02
	1.0	-114.85	-20.74	-6.28	-2.21	-0.79	-0.26	-0.09	-0.07	-0.09
		<i>C<sub>s</sub> Values</i>								
<i>A<sub>s</sub>/A<sub>c</sub></i>	<i>A<sub>b</sub>/A<sub>c</sub></i>	<i>Q<sub>s</sub>/Q<sub>c</sub></i>								
		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1	0.1	-3.90	-1.07	-0.04	0.66	1.27	1.87	2.47	3.10	3.76
	0.2	-3.76	-0.34	0.52	1.05	1.53	2.02	2.56	3.14	3.77
	0.3	-2.50	0.10	0.76	1.20	1.62	2.08	2.59	3.15	3.77
	0.4	-1.64	0.35	0.88	1.27	1.67	2.11	2.60	3.15	3.77
	0.5	-1.05	0.52	0.96	1.32	1.69	2.12	2.61	3.16	3.77
	0.6	-0.63	0.63	1.02	1.35	1.71	2.13	2.61	3.16	3.77
	0.7	-0.32	0.71	1.06	1.37	1.73	2.14	2.62	3.16	3.77
	0.8	-0.07	0.78	1.09	1.39	1.74	2.15	2.62	3.16	3.77
	0.9	0.13	0.83	1.11	1.40	1.74	2.15	2.62	3.16	3.77
	1.0	0.29	0.87	1.13	1.41	1.75	2.15	2.63	3.17	3.77
0.2	0.1	-14.54	-4.50	-1.82	-0.62	0.05	0.47	0.75	0.95	1.09
	0.2	-16.02	-3.15	-0.80	0.04	0.45	0.69	0.86	0.99	1.10
	0.3	-11.65	-1.94	-0.26	0.32	0.60	0.77	0.90	1.01	1.10
	0.4	-8.56	-1.20	0.05	0.47	0.68	0.82	0.92	1.02	1.11
	0.5	-6.41	-0.71	0.25	0.57	0.73	0.84	0.93	1.02	1.11
	0.6	-4.85	-0.36	0.38	0.63	0.76	0.86	0.94	1.02	1.11
	0.7	-3.68	-0.10	0.48	0.68	0.79	0.87	0.95	1.03	1.11
	0.8	-2.77	0.10	0.56	0.71	0.81	0.88	0.95	1.03	1.11
	0.9	-2.04	0.26	0.62	0.74	0.82	0.89	0.95	1.03	1.11
	1.0	-1.45	0.38	0.66	0.76	0.83	0.89	0.96	1.03	1.11
0.3	0.1	-32.30	-10.04	-4.34	-1.94	-0.73	-0.07	0.30	0.50	0.59
	0.2	-36.37	-7.59	-2.48	-0.79	-0.06	0.29	0.47	0.57	0.61
	0.3	-26.79	-5.07	-1.42	-0.27	0.21	0.42	0.53	0.59	0.61
	0.4	-19.94	-3.49	-0.80	0.02	0.35	0.49	0.56	0.60	0.62
	0.5	-15.18	-2.44	-0.41	0.20	0.43	0.54	0.58	0.61	0.62
	0.6	-11.73	-1.70	-0.13	0.32	0.49	0.56	0.60	0.61	0.62
	0.7	-9.13	-1.14	0.07	0.41	0.53	0.58	0.60	0.61	0.62
	0.8	-7.11	-0.72	0.23	0.48	0.57	0.60	0.61	0.62	0.62
	0.9	-5.49	-0.38	0.35	0.53	0.59	0.61	0.62	0.62	0.62
	1.0	-4.17	-0.11	0.45	0.58	0.61	0.62	0.62	0.62	0.62
0.4	0.1	-57.18	-17.78	-7.80	-3.69	-1.66	-0.59	-0.02	0.26	0.37
	0.2	-64.82	-13.76	-4.74	-1.81	-0.59	-0.02	0.24	0.36	0.39
	0.3	-47.92	-9.38	-2.93	-0.94	-0.16	0.19	0.34	0.39	0.40
	0.4	-35.81	-6.62	-1.88	-0.46	0.07	0.30	0.38	0.41	0.40
	0.5	-27.39	-4.78	-1.20	-0.16	0.22	0.36	0.41	0.42	0.41
	0.6	-21.28	-3.48	-0.73	0.04	0.31	0.41	0.43	0.43	0.41
	0.7	-16.68	-2.51	-0.38	0.20	0.38	0.44	0.45	0.43	0.41
	0.8	-13.10	-1.77	-0.12	0.31	0.44	0.46	0.46	0.44	0.41
	0.9	-10.24	-1.18	0.09	0.40	0.48	0.48	0.46	0.44	0.41
	1.0	-7.90	-0.69	0.26	0.47	0.51	0.50	0.47	0.44	0.41

ED5-1 Wye, 30 Degree, Converging (Continued)

		<i>C<sub>s</sub> Values (Concluded)</i>								
<i>A<sub>s</sub>/A<sub>c</sub></i>	<i>A<sub>b</sub>/A<sub>c</sub></i>	<i>Q<sub>b</sub>/Q<sub>c</sub></i>								
		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.5	0.1	-89.21	-27.74	-12.24	-5.89	-2.79	-1.18	-0.33	0.08	0.23
	0.2	-101.39	-21.64	-7.61	-3.07	-1.19	-0.34	0.05	0.22	0.26
	0.3	-75.05	-14.87	-4.83	-1.75	-0.54	-0.03	0.19	0.26	0.27
	0.4	-56.18	-10.59	-3.21	-1.02	-0.20	0.13	0.26	0.29	0.27
	0.5	-43.04	-7.74	-2.16	-0.56	0.02	0.23	0.30	0.30	0.27
	0.6	-33.51	-5.72	-1.43	-0.24	0.16	0.30	0.33	0.33	0.28
	0.7	-26.34	-4.22	-0.90	-0.01	0.27	0.35	0.35	0.32	0.28
	0.8	-20.75	-3.06	-0.49	0.16	0.35	0.39	0.37	0.33	0.28
	0.9	-16.29	-2.14	-0.17	0.30	0.41	0.41	0.38	0.33	0.28
	1.0	-12.64	-1.39	0.10	0.41	0.46	0.44	0.39	0.33	0.28
0.6	0.1	-128.36	-39.93	-17.66	-8.57	-4.15	-1.85	-0.66	-0.09	0.12
	0.2	-146.06	-31.26	-11.09	-4.56	-1.89	-0.68	-0.12	0.10	0.16
	0.3	-108.19	-21.55	-7.12	-2.69	-0.97	-0.24	0.07	0.17	0.17
	0.4	-81.04	-15.40	-4.80	-1.65	-0.48	-0.01	0.17	0.20	0.18
	0.5	-62.13	-11.31	-3.30	-0.99	-0.17	0.13	0.22	0.22	0.18
	0.6	-48.43	-8.41	-2.25	-0.54	0.03	0.22	0.26	0.24	0.18
	0.7	-38.10	-6.25	-1.49	-0.22	0.18	0.29	0.29	0.25	0.19
	0.8	-30.07	-4.59	-0.90	0.03	0.30	0.34	0.31	0.25	0.19
	0.9	-23.64	-3.27	-0.44	0.23	0.39	0.38	0.33	0.26	0.19
	1.0	-18.39	-2.20	-0.06	0.39	0.46	0.42	0.34	0.27	0.19
0.7	0.1	-174.66	-54.33	-24.05	-11.71	-5.72	-2.62	-1.01	-0.25	0.03
	0.2	-198.85	-42.62	-15.17	-6.31	-2.68	-1.04	-0.29	0.01	0.08
	0.3	-147.33	-29.41	-9.78	-3.77	-1.44	-0.45	-0.04	0.10	0.10
	0.4	-110.40	-21.07	-6.64	-2.36	-0.77	-0.14	0.09	0.15	0.11
	0.5	-84.67	-15.50	-4.60	-1.48	-0.36	0.05	0.17	0.17	0.11
	0.6	-66.02	-11.56	-3.19	-0.86	-0.08	0.18	0.23	0.19	0.12
	0.7	-51.97	-8.63	-2.15	-0.42	0.12	0.27	0.27	0.20	0.12
	0.8	-41.04	-6.37	-1.35	-0.08	0.27	0.34	0.29	0.21	0.12
	0.9	-32.30	-4.58	-0.72	0.19	0.39	0.39	0.32	0.22	0.12
	1.0	-25.16	-3.12	-0.21	0.40	0.49	0.43	0.33	0.23	0.13
0.8	0.1	-228.09	-70.95	-31.43	-15.33	-7.52	-3.48	-1.39	-0.40	-0.04
	0.2	-259.75	-55.70	-19.86	-8.29	-3.56	-1.43	-0.46	-0.06	-0.03
	0.3	-192.48	-38.47	-12.84	-4.99	-1.95	-0.66	-0.12	0.05	0.05
	0.4	-144.25	-27.58	-8.74	-3.16	-1.09	-0.26	0.05	0.11	0.06
	0.5	-110.65	-20.32	-6.08	-2.00	-0.55	-0.01	0.15	0.15	0.07
	0.6	-86.30	-15.17	-4.24	-1.20	-0.19	0.15	0.22	0.17	0.08
	0.7	-67.95	-11.34	-2.88	-0.62	0.08	0.27	0.27	0.19	0.08
	0.8	-53.67	-8.40	-1.84	-0.18	0.28	0.36	0.30	0.20	0.08
	0.9	-42.26	-6.05	-1.02	0.16	0.44	0.43	0.33	0.21	0.08
	1.0	-32.93	-4.15	-0.35	0.44	0.56	0.49	0.36	0.22	0.09
0.9	0.1	-288.66	-89.79	-39.78	-19.41	-9.54	-4.43	-1.80	-0.55	-0.09
	0.2	-328.76	-70.51	-25.16	-10.53	-4.54	-1.84	-0.62	-0.12	0.00
	0.3	-243.63	-48.72	-16.28	-6.35	-2.50	-0.87	-0.20	0.03	0.03
	0.4	-182.60	-34.94	-11.09	-4.03	-1.41	-0.37	0.02	0.10	0.04
	0.5	-140.07	-25.75	-7.74	-2.57	-0.74	-0.06	0.15	0.14	0.05
	0.6	-109.25	-19.24	-5.40	-1.56	-0.28	0.15	0.23	0.17	0.05
	0.7	-86.04	-14.40	-3.68	-0.83	0.06	0.30	0.30	0.20	0.06
	0.8	-67.96	-10.66	-2.37	-0.27	0.31	0.41	0.34	0.21	0.06
	0.9	-53.52	-7.70	-1.33	0.17	0.51	0.50	0.38	0.22	0.06
	1.0	-41.71	-5.29	-0.49	0.52	0.67	0.57	0.41	0.23	0.07
1.0	0.1	-356.36	-110.84	-49.12	-23.97	-11.78	-5.48	-2.23	-0.69	-0.12
	0.2	-405.88	-87.06	-31.07	-13.01	-5.62	-2.29	-0.77	-0.16	-0.02
	0.3	-300.78	-60.15	-20.11	-7.85	-3.10	-1.09	-0.26	0.02	0.02
	0.4	-225.44	-43.14	-13.70	-4.99	-1.76	-0.47	0.01	0.11	0.04
	0.5	-172.93	-31.80	-9.56	-3.18	-0.92	-0.09	0.17	0.17	0.05
	0.6	-134.89	-23.76	-6.68	-1.94	-0.35	0.17	0.28	0.20	0.06
	0.7	-106.23	-17.78	-4.56	-1.04	0.06	0.36	0.35	0.23	0.06
	0.8	-83.92	-13.18	-2.93	-0.35	0.37	0.50	0.41	0.25	0.06
	0.9	-66.08	-9.52	-1.65	0.19	0.62	0.61	0.46	0.26	0.07
	1.0	-51.51	-6.54	-0.61	0.63	0.81	0.70	0.49	0.28	0.07



ED5-2 Wye, 45 Degree, Converging



C<sub>b</sub> Values

A <sub>s</sub> /A <sub>c</sub>	A <sub>b</sub> /A <sub>c</sub>	C <sub>b</sub> Values								
		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1	0.1	-13.70	-1.90	-0.02	0.54	0.75	0.85	0.89	0.92	0.96
	0.2	-57.73	-10.44	-2.88	-0.64	0.22	0.59	0.76	0.85	0.94
	0.3	-131.08	-24.63	-7.59	-2.53	-0.60	0.24	0.61	0.79	0.92
	0.4	-233.78	-44.46	-14.15	-5.15	-1.71	-0.23	0.43	0.72	0.88
	0.5	-365.85	-69.96	-22.58	-8.50	-3.12	-0.81	0.21	0.65	0.82
	0.6	-527.21	-101.08	-32.83	-12.55	-4.80	-1.49	-0.02	0.59	0.79
	0.7	-717.81	-137.79	-44.90	-17.28	-6.74	-2.23	-0.23	0.60	0.85
	0.8	-937.72	-180.12	-58.79	-22.73	-8.96	-3.06	-0.45	0.63	0.95
	0.9	-1187.	-228.09	-74.53	-28.88	-11.45	-3.99	-0.69	0.67	1.07
	1.0	-1465.	-281.68	-92.10	-35.74	-14.23	-5.01	-0.94	0.74	1.22
0.2	0.1	-5.52	-0.26	0.56	0.79	0.88	0.92	0.95	0.97	1.05
	0.2	-25.19	-3.97	-0.64	0.32	0.67	0.82	0.90	0.96	1.08
	0.3	-58.03	-10.14	-2.63	-0.45	0.36	0.69	0.84	0.93	1.08
	0.4	-104.08	-18.80	-5.40	-1.51	-0.07	0.52	0.77	0.88	1.01
	0.5	-163.36	-29.97	-8.97	-2.87	-0.62	0.29	0.67	0.80	0.84
	0.6	-235.59	-43.47	-13.22	-4.44	-1.20	0.12	0.65	0.83	0.85
	0.7	-320.90	-59.38	-18.21	-6.25	-1.84	-0.04	0.68	0.91	0.93
	0.8	-419.32	-77.73	-23.95	-8.33	-2.56	-0.22	0.72	1.02	1.02
	0.9	-530.86	-98.50	-30.44	-10.66	-3.36	-0.40	0.79	1.16	1.14
	1.0	-655.51	-121.72	-37.68	-13.26	-4.25	-0.59	0.87	1.33	1.28
0.3	0.1	-2.74	0.32	0.78	0.90	0.94	0.97	0.99	1.02	1.13
	0.2	-14.27	-1.77	0.13	0.66	0.85	0.93	0.97	1.03	1.21
	0.3	-33.62	-5.28	-0.95	0.27	0.70	0.87	0.94	1.01	1.19
	0.4	-60.85	-10.26	-2.48	-0.30	0.47	0.77	0.88	0.93	1.04
	0.5	-95.87	-16.64	-4.44	-1.00	0.21	0.66	0.82	0.84	0.84
	0.6	-138.38	-24.26	-6.68	-1.73	0.01	0.66	0.88	0.91	0.88
	0.7	-188.60	-33.25	-9.32	-2.58	-0.20	0.68	0.98	1.02	0.95
	0.8	-246.54	-43.60	-12.34	-3.54	-0.43	0.72	1.11	1.15	1.03
	0.9	-312.21	-55.33	-15.76	-4.61	-0.68	0.78	1.26	1.31	1.13
	1.0	-385.59	-68.43	-19.56	-5.79	-0.94	0.86	1.45	1.49	1.24
0.4	0.1	-1.32	0.63	0.90	0.96	0.99	1.00	1.02	1.06	1.20
	0.2	-8.77	-0.64	0.54	0.85	0.95	0.99	1.03	1.09	1.31
	0.3	-21.41	-2.85	-0.10	0.63	0.87	0.96	1.00	1.06	1.26
	0.4	-39.30	-6.02	-1.05	0.28	0.72	0.87	0.91	0.92	1.00
	0.5	-62.10	-9.96	-2.16	-0.06	0.63	0.85	0.90	0.88	0.86
	0.6	-89.77	-14.65	-3.42	-0.38	0.61	0.93	0.99	0.95	0.90
	0.7	-122.46	-20.19	-4.88	-0.74	0.61	1.04	1.12	1.06	0.95
	0.8	-160.18	-26.56	-6.55	-1.15	0.62	1.18	1.29	1.19	1.01
	0.9	-202.93	-33.77	-8.44	-1.60	0.64	1.36	1.48	1.35	1.07
	1.0	-250.70	-41.83	-10.54	-2.09	0.68	1.56	1.71	1.53	1.15
0.5	0.1	-0.44	0.83	0.98	1.01	1.02	1.03	1.05	1.10	1.27
	0.2	-5.45	0.04	0.79	0.97	1.02	1.04	1.07	1.14	1.39
	0.3	-14.10	-1.39	0.40	0.84	0.97	1.00	1.02	1.07	1.28
	0.4	-26.48	-3.53	-0.24	0.59	0.83	0.89	0.88	0.85	0.86
	0.5	-41.84	-5.96	-0.80	0.51	0.88	0.97	0.95	0.90	0.87
	0.6	-60.61	-8.90	-1.46	0.43	0.97	1.09	1.06	0.97	0.90
	0.7	-82.80	-12.36	-2.22	0.35	1.09	1.25	1.20	1.08	0.93
	0.8	-108.39	-16.35	-3.09	0.27	1.24	1.45	1.38	1.20	0.96
	0.9	-137.41	-20.86	-4.07	0.19	1.42	1.68	1.59	1.35	0.99
	1.0	-169.84	-25.90	-5.15	0.11	1.63	1.95	1.83	1.52	1.02
0.6	0.1	-0.41	0.83	0.98	1.02	1.03	1.04	1.07	1.13	1.33
	0.2	-5.54	-0.08	0.70	0.91	0.98	1.01	1.05	1.14	1.42
	0.3	-14.48	-1.75	0.13	0.64	0.81	0.88	0.92	0.98	1.19
	0.4	-27.10	-4.14	-0.68	0.26	0.57	0.68	0.71	0.72	0.76
	0.5	-42.84	-6.91	-1.50	-0.02	0.47	0.64	0.68	0.69	0.70
	0.6	-62.07	-10.28	-2.48	-0.34	0.37	0.61	0.67	0.66	0.63
	0.7	-84.79	-14.26	-3.62	-0.71	0.27	0.59	0.67	0.63	0.54
	0.8	-111.02	-18.84	-4.92	-1.12	0.16	0.58	0.67	0.61	0.44
	0.9	-140.76	-24.03	-6.40	-1.57	0.04	0.58	0.68	0.59	0.31
	1.0	-174.01	-29.83	-8.04	-2.07	-0.08	0.58	0.70	0.56	0.15

ED5-2 Wye, 45 Degree, Converging (Continued)

		<i>C<sub>b</sub> Values (Concluded)</i>								
<i>A<sub>s</sub>/A<sub>c</sub></i>	<i>A<sub>b</sub>/A<sub>c</sub></i>	<i>Q<sub>b</sub>/Q<sub>c</sub></i>								
		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.7	0.1	0.03	0.94	1.03	1.05	1.06	1.07	1.10	1.16	1.39
	0.2	-3.96	0.25	0.83	0.97	1.01	1.04	1.08	1.17	1.47
	0.3	-11.07	-1.10	0.34	0.71	0.83	0.87	0.90	0.95	1.13
	0.4	-20.92	-2.92	-0.27	0.43	0.65	0.72	0.73	0.73	0.77
	0.5	-33.20	-5.01	-0.85	0.24	0.59	0.69	0.71	0.69	0.70
	0.6	-48.21	-7.55	-1.55	0.03	0.53	0.68	0.69	0.65	0.61
	0.7	-65.95	-10.56	-2.37	-0.20	0.48	0.68	0.69	0.62	0.49
	0.8	-86.42	-14.01	-3.30	-0.46	0.43	0.68	0.69	0.58	0.35
	0.9	-109.65	-17.93	-4.35	-0.75	0.38	0.70	0.70	0.53	0.18
	1.0	-135.63	-22.32	-5.53	-1.07	0.33	0.72	0.71	0.48	-0.03
0.8	0.1	0.38	1.02	1.08	1.08	1.08	1.09	1.12	1.19	1.44
	0.2	-2.78	0.50	0.91	1.01	1.03	1.05	1.09	1.18	1.49
	0.3	-8.58	-0.65	0.47	0.74	0.82	0.85	0.86	0.89	1.02
	0.4	-16.29	-2.00	0.05	0.56	0.71	0.75	0.74	0.74	0.78
	0.5	-25.98	-3.59	-0.37	0.44	0.68	0.73	0.72	0.69	0.69
	0.6	-37.82	-5.52	-0.87	0.31	0.65	0.72	0.70	0.64	0.58
	0.7	-51.83	-7.79	-1.44	0.17	0.63	0.73	0.69	0.59	0.43
	0.8	-68.01	-10.42	-2.10	0.01	0.62	0.75	0.69	0.53	0.25
	0.9	-86.37	-13.39	-2.84	-0.16	0.61	0.77	0.68	0.47	0.03
	1.0	-106.91	-16.73	-3.68	-0.35	0.61	0.79	0.68	0.38	-0.25
0.9	0.1	0.65	1.10	1.11	1.10	1.10	1.11	1.14	1.22	1.49
	0.2	-1.87	0.68	0.98	1.03	1.05	1.06	1.09	1.18	1.49
	0.3	-6.70	-0.33	0.54	0.74	0.79	0.80	0.80	0.81	0.87
	0.4	-12.69	-1.29	0.29	0.66	0.76	0.77	0.75	0.74	0.78
	0.5	-20.37	-2.48	0.00	0.59	0.74	0.75	0.72	0.69	0.67
	0.6	-29.77	-3.94	-0.34	0.52	0.73	0.75	0.70	0.63	0.54
	0.7	-40.89	-5.66	-0.73	0.45	0.74	0.76	0.68	0.56	0.36
	0.8	-53.74	-7.64	-1.18	0.37	0.76	0.78	0.67	0.48	0.13
	0.9	-68.32	-9.89	-1.69	0.28	0.77	0.80	0.65	0.38	-0.15
	1.0	-84.66	-12.42	-2.27	0.18	0.80	0.83	0.62	0.26	-0.49
1.0	0.1	0.88	1.16	1.14	1.12	1.12	1.13	1.16	1.25	1.54
	0.2	-1.17	0.81	1.02	1.05	1.05	1.06	1.09	1.18	1.48
	0.3	-5.09	-0.02	0.64	0.78	0.81	0.81	0.80	0.80	0.86
	0.4	-9.81	-0.72	0.48	0.74	0.79	0.78	0.76	0.74	0.77
	0.5	-15.89	-1.61	0.29	0.71	0.79	0.77	0.72	0.68	0.65
	0.6	-23.34	-2.69	0.07	0.68	0.80	0.77	0.69	0.60	0.49
	0.7	-32.15	-3.96	-0.18	0.66	0.82	0.78	0.67	0.51	0.27
	0.8	-42.35	-5.44	-0.47	0.64	0.85	0.79	0.63	0.41	0.00
	0.9	-53.94	-7.12	-0.80	0.61	0.88	0.81	0.60	0.28	-0.34
	1.0	-66.93	-9.01	-1.17	0.58	0.92	0.82	0.55	0.13	-0.75

		<i>C<sub>s</sub> Values</i>								
<i>A<sub>s</sub>/A<sub>c</sub></i>	<i>A<sub>b</sub>/A<sub>c</sub></i>	<i>Q<sub>s</sub>/Q<sub>c</sub></i>								
		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1	0.1	-0.64	-0.63	0.17	1.00	1.87	2.79	3.76	4.81	5.92
	0.2	-2.38	-0.06	0.77	1.47	2.19	2.99	3.88	4.86	5.93
	0.3	-1.56	0.35	1.03	1.64	2.30	3.06	3.91	4.87	5.94
	0.4	-0.89	0.59	1.17	1.73	2.36	3.09	3.93	4.88	5.94
	0.5	-0.40	0.75	1.26	1.78	2.40	3.11	3.94	4.88	5.94
	0.6	-0.04	0.86	1.32	1.82	2.42	3.13	3.95	4.89	5.94
	0.7	0.23	0.95	1.36	1.85	2.44	3.14	3.96	4.89	5.94
	0.8	0.45	1.01	1.40	1.87	2.45	3.15	3.96	4.89	5.94
	0.9	0.62	1.06	1.42	1.88	2.46	3.15	3.96	4.89	5.94
	1.0	0.76	1.10	1.44	1.89	2.47	3.16	3.97	4.89	5.94
0.2	0.1	-0.33	-2.09	-1.13	-0.35	0.22	0.65	0.97	1.23	1.45
	0.2	-10.16	-2.08	-0.43	0.24	0.62	0.88	1.10	1.29	1.46
	0.3	-7.83	-1.20	0.03	0.50	0.77	0.97	1.14	1.30	1.46
	0.4	-5.62	-0.59	0.30	0.65	0.85	1.01	1.16	1.31	1.46
	0.5	-3.96	-0.18	0.48	0.74	0.90	1.04	1.18	1.32	1.47
	0.6	-2.71	0.12	0.60	0.80	0.94	1.06	1.19	1.32	1.47
	0.7	-1.75	0.34	0.70	0.85	0.96	1.07	1.19	1.32	1.47
	0.8	-0.99	0.52	0.77	0.88	0.98	1.08	1.20	1.32	1.47
	0.9	-0.38	0.66	0.82	0.91	0.99	1.09	1.20	1.33	1.47
	1.0	0.13	0.77	0.87	0.93	1.00	1.10	1.20	1.33	1.47

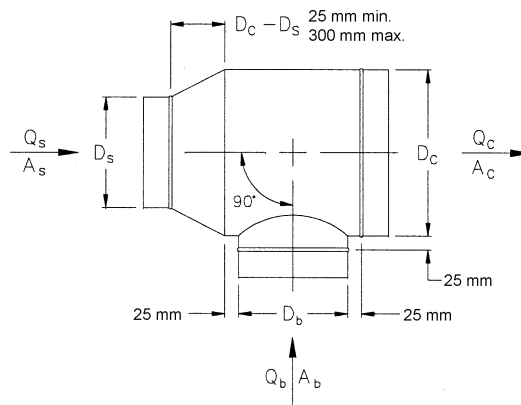
## ED5-2 Wye, 45 Degree, Converging (Continued)

		$C_s$ Values (Continued)								
		$Q_s/Q_c$								
$A_s/A_c$	$A_p/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.3	0.1	-0.18	-4.36	-2.61	-1.29	-0.45	0.08	0.41	0.60	0.71
	0.2	-23.33	-5.14	-1.67	-0.44	0.12	0.42	0.58	0.67	0.72
	0.3	-18.44	-3.44	-0.84	0.00	0.36	0.54	0.64	0.69	0.73
	0.4	-13.64	-2.22	-0.34	0.25	0.49	0.60	0.67	0.70	0.73
	0.5	-10.00	-1.37	0.00	0.41	0.57	0.64	0.69	0.71	0.73
	0.6	-7.26	-0.75	0.24	0.52	0.62	0.67	0.70	0.72	0.73
	0.7	-5.15	-0.29	0.41	0.60	0.66	0.69	0.71	0.72	0.73
	0.8	-3.48	0.07	0.55	0.66	0.69	0.70	0.71	0.72	0.73
	0.9	-2.14	0.36	0.65	0.71	0.72	0.72	0.72	0.72	0.73
	1.0	-1.03	0.60	0.74	0.75	0.73	0.73	0.72	0.72	0.73
0.4	0.1	-0.46	-7.64	-4.66	-2.49	-1.15	-0.36	0.10	0.33	0.43
	0.2	-42.17	-9.48	-3.34	-1.23	-0.31	0.12	0.33	0.42	0.44
	0.3	-33.68	-6.60	-1.98	-0.53	0.05	0.31	0.41	0.45	0.45
	0.4	-25.24	-4.51	-1.13	-0.13	0.25	0.40	0.46	0.47	0.45
	0.5	-18.83	-3.04	-0.57	0.13	0.37	0.46	0.48	0.48	0.46
	0.6	-13.99	-1.97	-0.17	0.31	0.46	0.50	0.50	0.48	0.46
	0.7	-10.27	-1.17	0.12	0.44	0.52	0.53	0.51	0.49	0.46
	0.8	-7.32	-0.54	0.35	0.54	0.57	0.55	0.52	0.49	0.46
	0.9	-4.94	-0.04	0.53	0.62	0.61	0.57	0.53	0.49	0.46
	1.0	-2.98	0.37	0.68	0.68	0.64	0.58	0.54	0.50	0.46
0.5	0.1	-1.43	-12.03	-7.36	-4.03	-2.01	-0.84	-0.18	0.14	0.26
	0.2	-66.95	-15.18	-5.49	-2.21	-0.81	-0.16	0.14	0.26	0.28
	0.3	-53.80	-10.77	-3.45	-1.17	-0.27	0.11	0.26	0.30	0.29
	0.4	-40.66	-7.54	-2.16	-0.57	0.02	0.25	0.32	0.33	0.30
	0.5	-30.68	-5.27	-1.30	-0.18	0.21	0.33	0.36	0.34	0.30
	0.6	-23.15	-3.62	-0.69	0.09	0.33	0.39	0.38	0.35	0.30
	0.7	-17.34	-2.38	-0.24	0.29	0.42	0.43	0.40	0.35	0.30
	0.8	-12.75	-1.41	0.11	0.44	0.49	0.47	0.41	0.36	0.30
	0.9	-9.04	-0.64	0.39	0.56	0.55	0.49	0.43	0.36	0.30
	1.0	-5.99	0.00	0.61	0.65	0.59	0.51	0.43	0.36	0.30
0.6	0.1	-3.34	-17.58	-10.74	-5.94	-3.06	-1.39	-0.48	-0.03	0.13
	0.2	-97.90	-22.29	-8.18	-3.41	-1.39	-0.46	-0.03	0.13	0.16
	0.3	-79.03	-15.99	-5.28	-1.94	-0.64	-0.09	0.13	0.19	0.17
	0.4	-60.15	-11.37	-3.44	-1.09	-0.23	0.10	0.21	0.22	0.18
	0.5	-45.80	-8.13	-2.22	-0.55	0.03	0.22	0.26	0.24	0.18
	0.6	-34.97	-5.77	-1.35	-0.17	0.20	0.30	0.30	0.25	0.18
	0.7	-26.62	-3.98	-0.71	0.11	0.33	0.36	0.32	0.26	0.19
	0.8	-20.02	-2.59	-0.21	0.33	0.43	0.41	0.34	0.26	0.19
	0.9	-14.68	-1.48	0.18	0.49	0.51	0.44	0.35	0.27	0.19
	1.0	-10.29	-0.57	0.51	0.63	0.57	0.47	0.37	0.27	0.19
0.7	0.1	-6.43	-24.36	-14.82	-8.23	-4.31	-2.04	-0.81	-0.20	0.01
	0.2	-135.28	-30.88	-11.42	-4.85	-2.08	-0.80	-0.21	0.02	0.06
	0.3	-109.64	-22.35	-7.50	-2.88	-1.07	-0.31	0.00	0.09	0.07
	0.4	-83.96	-16.08	-5.02	-1.73	-0.52	-0.05	0.11	0.13	0.08
	0.5	-64.44	-11.67	-3.36	-0.99	-0.17	0.11	0.18	0.15	0.09
	0.6	-49.71	-8.47	-2.19	-0.48	0.06	0.22	0.22	0.17	0.09
	0.7	-38.35	-6.04	-1.31	-0.10	0.24	0.30	0.26	0.18	0.09
	0.8	-29.37	-4.16	-0.64	0.18	0.37	0.36	0.28	0.19	0.09
	0.9	-22.12	-2.65	-0.10	0.41	0.47	0.40	0.30	0.19	0.09
	1.0	-16.14	-1.41	0.33	0.60	0.55	0.44	0.32	0.20	0.09
0.8	0.1	-10.94	-32.43	-19.63	-10.93	-5.77	-2.80	-1.18	-0.38	-0.09
	0.2	-179.32	-41.01	-15.25	-6.55	-2.88	-1.19	-0.41	-0.10	-0.04
	0.3	-145.86	-29.89	-10.14	-3.99	-1.58	-0.55	-0.13	0.00	-0.02
	0.4	-112.34	-21.71	-6.91	-2.50	-0.86	-0.22	0.01	0.05	-0.01
	0.5	-86.85	-15.96	-4.75	-1.54	-0.41	-0.01	0.10	0.08	0.00
	0.6	-67.62	-11.78	-3.22	-0.87	-0.10	0.13	0.16	0.10	0.00
	0.7	-52.79	-8.62	-2.08	-0.38	0.12	0.23	0.20	0.11	0.00
	0.8	-41.06	-6.16	-1.20	0.00	0.29	0.31	0.23	0.12	0.01
	0.9	-31.59	-4.19	-0.51	0.29	0.43	0.37	0.26	0.13	0.01
	1.0	-23.78	-2.58	0.06	0.53	0.54	0.42	0.28	0.14	0.01

ED5-2 Wye, 45 Degree, Converging (Continued)

		<i>C<sub>s</sub> Values (Concluded)</i>								
		<i>Q<sub>s</sub>/Q<sub>c</sub></i>								
<i>A<sub>s</sub>/A<sub>c</sub></i>	<i>A<sub>b</sub>/A<sub>c</sub></i>	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.9	0.1	-17.13	-41.85	-25.21	-14.05	-7.45	-3.66	-1.59	-0.57	-0.20
	0.2	-230.27	-52.75	-19.69	-8.53	-3.81	-1.63	-0.63	-0.22	-0.13
	0.3	-187.95	-38.69	-13.24	-5.29	-2.16	-0.83	-0.28	-0.10	-0.10
	0.4	-145.53	-28.34	-9.15	-3.41	-1.26	-0.41	-0.10	-0.04	-0.09
	0.5	-113.27	-21.07	-6.42	-2.19	-0.69	-0.15	0.01	0.00	-0.09
	0.6	-88.94	-15.78	-4.48	-1.35	-0.30	0.03	0.09	0.03	-0.08
	0.7	-70.16	-11.78	-3.04	-0.73	-0.02	0.16	0.14	0.04	-0.08
	0.8	-55.33	-8.67	-1.93	-0.25	0.20	0.26	0.18	0.06	-0.07
	0.9	-43.33	-6.18	-1.05	0.12	0.37	0.33	0.21	0.07	-0.07
1.0	-33.46	-4.14	-0.34	0.42	0.50	0.39	0.24	0.08	-0.07	
1.0	0.1	-25.23	-52.69	-31.58	-17.61	-9.37	-4.64	-2.06	-0.79	-0.31
	0.2	-288.39	-66.15	-24.77	-10.80	-4.88	-2.14	-0.87	-0.35	-0.22
	0.3	-236.14	-48.79	-16.81	-6.80	-2.85	-1.15	-0.44	-0.20	-0.19
	0.4	-183.77	-36.02	-11.76	-4.47	-1.73	-0.63	-0.22	-0.12	-0.18
	0.5	-143.95	-27.05	-8.39	-2.98	-1.03	-0.31	-0.08	-0.08	-0.17
	0.6	-113.91	-20.52	-6.00	-1.93	-0.55	-0.09	0.01	-0.04	-0.16
	0.7	-90.73	-15.58	-4.23	-1.17	-0.20	0.07	0.08	-0.02	-0.16
	0.8	-72.41	-11.74	-2.86	-0.58	0.06	0.19	0.13	-0.01	-0.16
	0.9	-57.61	-8.66	-1.77	-0.12	0.27	0.28	0.16	0.01	-0.15
	1.0	-45.42	-6.15	-0.88	0.25	0.44	0.36	0.20	0.02	-0.15

ED5-3 Tee, *D<sub>c</sub> < or = 250 mm*, Converging



		<i>C<sub>b</sub> Values</i>								
		<i>Q<sub>b</sub>/Q<sub>c</sub></i>								
<i>A<sub>s</sub>/A<sub>c</sub></i>	<i>A<sub>b</sub>/A<sub>c</sub></i>	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1	0.1	-13.39	-1.73	0.13	0.68	0.89	0.98	1.02	1.05	1.08
	0.2	-56.68	-9.99	-2.53	-0.32	0.52	0.88	1.04	1.12	1.18
	0.3	-128.89	-23.79	-6.99	-2.02	-0.12	0.68	1.04	1.20	1.29
	0.4	-230.03	-43.12	-13.26	-4.40	-1.04	0.40	1.03	1.30	1.42
	0.5	-360.10	-68.01	-21.33	-7.49	-2.23	0.02	1.00	1.40	1.53
	0.6	-519.10	-98.44	-31.20	-11.27	-3.69	-0.46	0.95	1.52	1.66
	0.7	-706.92	-134.35	-42.83	-15.70	-5.38	-0.99	0.93	1.70	1.88
	0.8	-923.64	-175.79	-56.25	-20.82	-7.34	-1.60	0.90	1.91	2.15
	0.9	-1169.	-222.75	-71.47	-26.62	-9.56	-2.30	0.87	2.14	2.44
	1.0	-1444.	-275.24	-88.47	-33.10	-12.04	-3.08	0.84	2.40	2.76
0.2	0.1	-5.33	-0.12	0.69	0.92	1.01	1.04	1.06	1.08	1.13
	0.2	-24.56	-3.63	-0.36	0.59	0.93	1.08	1.14	1.19	1.27
	0.3	-56.72	-9.54	-2.15	-0.01	0.78	1.10	1.23	1.30	1.39
	0.4	-101.83	-17.86	-4.68	-0.87	0.52	1.09	1.32	1.41	1.48
	0.5	-159.91	-28.59	-7.98	-2.02	0.17	1.05	1.40	1.51	1.51
	0.6	-230.83	-41.68	-11.98	-3.39	-0.24	1.03	1.53	1.66	1.61
	0.7	-314.56	-57.10	-16.68	-4.98	-0.69	1.04	1.71	1.90	1.82
	0.8	-411.18	-74.90	-22.10	-6.82	-1.21	1.04	1.92	2.16	2.05
	0.9	-520.69	-95.08	-28.25	-8.90	-1.81	1.04	2.15	2.45	2.31
	1.0	-643.09	-117.63	-35.12	-11.24	-2.47	1.04	2.41	2.78	2.58

ED5-3 Tee,  $D_c < \text{or} = 250 \text{ mm}$ , Converging (Continued)

		$C_b$ Values (Continued)								
		$Q_b/Q_c$								
$A_s/A_c$	$A_b/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.3	0.1	-2.67	0.42	0.88	1.01	1.05	1.07	1.09	1.11	1.18
	0.2	-14.05	-1.55	0.36	0.89	1.08	1.16	1.19	1.23	1.34
	0.3	-33.18	-4.91	-0.58	0.64	1.07	1.23	1.30	1.34	1.44
	0.4	-60.09	-9.68	-1.94	0.24	1.00	1.29	1.39	1.42	1.47
	0.5	-94.80	-15.89	-3.74	-0.33	0.87	1.32	1.46	1.46	1.38
	0.6	-136.97	-23.33	-5.84	-0.92	0.81	1.45	1.65	1.66	1.53
	0.7	-186.81	-32.14	-8.32	-1.62	0.74	1.61	1.88	1.88	1.70
	0.8	-244.33	-42.30	-11.19	-2.43	0.65	1.78	2.14	2.13	1.88
	0.9	-309.54	-53.82	-14.44	-3.35	0.54	1.98	2.42	2.41	2.08
	1.0	-382.43	-66.70	-18.08	-4.39	0.42	2.19	2.74	2.72	2.29
0.4	0.1	-1.36	0.69	0.98	1.06	1.08	1.10	1.11	1.14	1.23
	0.2	-8.95	-0.54	0.71	1.04	1.15	1.20	1.22	1.26	1.40
	0.3	-21.82	-2.70	0.16	0.94	1.19	1.29	1.32	1.35	1.47
	0.4	-39.99	-5.81	-0.67	0.73	1.19	1.35	1.39	1.39	1.41
	0.5	-63.37	-9.82	-1.75	0.45	1.18	1.42	1.47	1.43	1.32
	0.6	-91.72	-14.59	-2.97	0.20	1.26	1.60	1.67	1.60	1.43
	0.7	-125.23	-20.24	-4.41	-0.10	1.34	1.81	1.90	1.81	1.56
	0.8	-163.91	-26.77	-6.09	-0.45	1.43	2.04	2.16	2.03	1.69
	0.9	-207.76	-34.17	-7.99	-0.85	1.53	2.30	2.44	2.28	1.82
	1.0	-256.79	-42.45	-10.12	-1.30	1.63	2.58	2.75	2.54	1.95
0.5	0.1	-0.60	0.85	1.04	1.09	1.11	1.12	1.13	1.16	1.27
	0.2	-6.03	0.04	0.91	1.13	1.20	1.22	1.24	1.29	1.44
	0.3	-15.35	-1.46	0.56	1.09	1.25	1.30	1.32	1.35	1.46
	0.4	-28.59	-3.67	-0.01	0.96	1.26	1.34	1.35	1.32	1.29
	0.5	-45.45	-6.42	-0.66	0.85	1.33	1.45	1.45	1.38	1.24
	0.6	-65.92	-9.70	-1.41	0.78	1.46	1.64	1.63	1.53	1.32
	0.7	-90.12	-13.58	-2.29	0.69	1.61	1.86	1.85	1.70	1.39
	0.8	-118.07	-18.07	-3.32	0.57	1.78	2.11	2.09	1.89	1.46
	0.9	-149.75	-23.18	-4.49	0.43	1.96	2.38	2.35	2.09	1.53
	1.0	-185.19	-28.89	-5.81	0.27	2.16	2.67	2.63	2.31	1.57
0.6	0.1	-0.11	0.96	1.09	1.12	1.12	1.13	1.15	1.18	1.31
	0.2	-4.20	0.39	1.03	1.18	1.22	1.24	1.26	1.30	1.47
	0.3	-11.33	-0.72	0.79	1.16	1.27	1.30	1.31	1.33	1.43
	0.4	-21.57	-2.42	0.35	1.05	1.25	1.29	1.27	1.22	1.12
	0.5	-34.29	-4.35	-0.03	1.07	1.38	1.44	1.41	1.32	1.16
	0.6	-49.85	-6.73	-0.50	1.08	1.54	1.63	1.57	1.45	1.19
	0.7	-68.26	-9.55	-1.06	1.09	1.71	1.83	1.76	1.58	1.21
	0.8	-89.52	-12.81	-1.72	1.10	1.91	2.07	1.97	1.73	1.22
	0.9	-113.64	-16.52	-2.47	1.10	2.12	2.32	2.20	1.88	1.21
	1.0	-140.62	-20.68	-3.33	1.09	2.35	2.60	2.44	2.03	1.16
0.7	0.1	0.22	1.03	1.12	1.14	1.14	1.14	1.16	1.20	1.35
	0.2	-3.00	0.62	1.10	1.21	1.23	1.24	1.26	1.31	1.49
	0.3	-8.74	-0.27	0.91	1.19	1.26	1.27	1.27	1.28	1.36
	0.4	-16.90	-1.59	0.58	1.11	1.25	1.27	1.24	1.18	1.06
	0.5	-26.99	-3.06	0.33	1.17	1.38	1.41	1.36	1.26	1.06
	0.6	-39.35	-4.86	0.02	1.22	1.54	1.57	1.50	1.35	1.05
	0.7	-53.97	-7.01	-0.35	1.29	1.72	1.76	1.65	1.45	1.02
	0.8	-70.87	-9.50	-0.79	1.35	1.91	1.97	1.82	1.54	0.96
	0.9	-90.04	-12.34	-1.31	1.41	2.12	2.19	2.00	1.64	0.86
	1.0	-111.50	-15.53	-1.89	1.46	2.34	2.43	2.19	1.73	0.72
0.8	0.1	0.46	1.08	1.14	1.15	1.15	1.16	1.17	1.22	1.38
	0.2	-2.20	0.76	1.14	1.22	1.24	1.24	1.26	1.31	1.49
	0.3	-7.04	-0.01	0.95	1.18	1.23	1.23	1.23	1.22	1.27
	0.4	-13.77	-1.06	0.71	1.13	1.24	1.24	1.20	1.13	1.00
	0.5	-22.11	-2.24	0.54	1.20	1.36	1.36	1.30	1.19	0.97
	0.6	-32.33	-3.69	0.31	1.27	1.50	1.50	1.41	1.25	0.90
	0.7	-44.42	-5.41	0.04	1.34	1.66	1.65	1.53	1.30	0.81
	0.8	-58.40	-7.42	-0.29	1.42	1.83	1.83	1.65	1.35	0.67
	0.9	-74.28	-9.72	-0.67	1.49	2.01	2.01	1.78	1.38	0.49
	1.0	-92.06	-12.30	-1.12	1.56	2.21	2.20	1.92	1.40	0.24

ED5-3 Tee,  $D_c \leq 250$  mm, Converging (Continued)

		$C_b$ Values (Concluded)								
		$Q_b/Q_c$								
$A_s/A_c$	$A_b/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.9	0.1	0.62	1.12	1.16	1.16	1.16	1.17	1.19	1.24	1.41
	0.2	-1.67	0.85	1.16	1.22	1.23	1.24	1.25	1.30	1.48
	0.3	-5.95	0.12	0.95	1.14	1.18	1.18	1.16	1.15	1.14
	0.4	-11.68	-0.74	0.77	1.12	1.20	1.20	1.16	1.08	0.93
	0.5	-18.85	-1.74	0.63	1.18	1.31	1.30	1.23	1.11	0.86
	0.6	-27.63	-2.98	0.44	1.24	1.42	1.41	1.31	1.13	0.75
	0.7	-38.04	-4.45	0.21	1.30	1.55	1.53	1.39	1.14	0.58
	0.8	-50.07	-6.17	-0.07	1.36	1.69	1.66	1.47	1.13	0.37
	0.9	-63.75	-8.14	-0.40	1.42	1.83	1.79	1.54	1.11	0.09
	1.0	-79.08	-10.36	-0.79	1.46	1.98	1.92	1.61	1.06	-0.26
1.0	0.1	0.74	1.15	1.18	1.17	1.17	1.18	1.20	1.25	1.43
	0.2	-1.33	0.89	1.16	1.21	1.22	1.22	1.24	1.29	1.46
	0.3	-5.30	0.15	0.90	1.08	1.11	1.11	1.09	1.06	0.99
	0.4	-10.31	-0.57	0.78	1.09	1.16	1.15	1.11	1.03	0.86
	0.5	-16.71	-1.47	0.64	1.13	1.24	1.22	1.15	1.03	0.74
	0.6	-24.56	-2.59	0.46	1.17	1.32	1.30	1.20	1.01	0.57
	0.7	-33.87	-3.93	0.23	1.20	1.41	1.38	1.24	0.97	0.34
	0.8	-44.64	-5.49	-0.05	1.22	1.51	1.46	1.27	0.91	0.05
	0.9	-56.89	-7.29	-0.38	1.24	1.59	1.54	1.28	0.82	-0.33
	1.0	-70.62	-9.32	-0.77	1.24	1.68	1.61	1.28	0.69	-0.80
		$C_s$ Values								
		$Q_s/Q_c$								
$A_s/A_c$	$A_b/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1	0.1	6.57	1.67	1.10	0.95	0.88	0.85	0.84	0.83	0.82
	0.2	4.13	1.39	1.03	0.92	0.87	0.85	0.83	0.83	0.82
	0.3	3.30	1.30	1.00	0.91	0.87	0.85	0.83	0.82	0.82
	0.4	2.89	1.24	0.99	0.90	0.86	0.84	0.83	0.82	0.82
	0.5	2.63	1.21	0.97	0.90	0.86	0.84	0.83	0.82	0.82
	0.6	2.45	1.18	0.97	0.89	0.86	0.84	0.83	0.82	0.82
	0.7	2.32	1.16	0.96	0.89	0.86	0.84	0.83	0.82	0.82
	0.8	2.22	1.15	0.95	0.89	0.85	0.84	0.83	0.82	0.82
	0.9	2.14	1.13	0.95	0.88	0.85	0.84	0.83	0.82	0.82
	1.0	2.07	1.12	0.94	0.88	0.85	0.84	0.83	0.82	0.82
0.2	0.1	34.53	5.26	2.11	1.29	0.98	0.84	0.76	0.71	0.68
	0.2	18.11	3.42	1.62	1.11	0.90	0.80	0.74	0.70	0.68
	0.3	12.67	2.79	1.45	1.04	0.87	0.78	0.73	0.70	0.68
	0.4	9.98	2.47	1.36	1.01	0.85	0.77	0.72	0.69	0.67
	0.5	8.39	2.27	1.30	0.98	0.84	0.76	0.72	0.69	0.67
	0.6	7.34	2.13	1.26	0.96	0.83	0.76	0.72	0.69	0.67
	0.7	6.61	2.02	1.22	0.95	0.82	0.75	0.71	0.69	0.67
	0.8	6.08	1.94	1.19	0.93	0.81	0.75	0.71	0.68	0.67
	0.9	5.68	1.87	1.17	0.92	0.80	0.74	0.70	0.68	0.66
	1.0	4.55	1.61	1.05	0.86	0.76	0.71	0.68	0.66	0.65
0.3	0.1	90.35	12.35	4.15	2.07	1.30	0.95	0.76	0.65	0.59
	0.2	44.33	7.19	2.80	1.57	1.08	0.84	0.71	0.63	0.57
	0.3	29.24	5.46	2.33	1.40	1.00	0.80	0.69	0.62	0.57
	0.4	21.88	4.59	2.09	1.30	0.96	0.78	0.67	0.61	0.56
	0.5	17.62	4.06	1.93	1.24	0.92	0.76	0.66	0.60	0.56
	0.6	14.90	3.71	1.82	1.19	0.90	0.74	0.65	0.59	0.55
	0.7	13.06	3.45	1.74	1.15	0.88	0.73	0.64	0.59	0.55
	0.8	11.78	3.26	1.67	1.12	0.86	0.72	0.63	0.58	0.54
	0.9	9.02	2.64	1.41	0.97	0.77	0.66	0.59	0.54	0.51
	1.0	8.36	2.52	1.36	0.95	0.75	0.65	0.58	0.54	0.51
0.4	0.1	167.76	22.21	7.04	3.22	1.81	1.17	0.84	0.64	0.52
	0.2	78.99	12.25	4.42	2.26	1.39	0.97	0.74	0.60	0.50
	0.3	50.14	8.96	3.54	1.92	1.24	0.90	0.70	0.57	0.49
	0.4	36.26	7.32	3.08	1.74	1.16	0.85	0.67	0.56	0.48
	0.5	28.38	6.35	2.80	1.63	1.10	0.82	0.65	0.54	0.47
	0.6	23.50	5.72	2.61	1.54	1.05	0.79	0.63	0.53	0.46
	0.7	20.32	5.27	2.46	1.47	1.02	0.77	0.62	0.52	0.45
	0.8	14.94	4.13	1.98	1.21	0.85	0.65	0.53	0.46	0.40
	0.9	13.55	3.88	1.89	1.16	0.82	0.63	0.52	0.45	0.39
	1.0	12.66	3.69	1.80	1.12	0.79	0.62	0.51	0.44	0.39

ED5-3 Tee,  $D_c < \text{or} = 250 \text{ mm}$ , Converging (Continued)

		$C_s$ Values (Concluded)								
		$Q_s/Q_c$								
$A_s/A_c$	$A_b/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.5	0.1	252.09	33.17	10.32	4.56	2.44	1.47	0.97	0.67	0.49
	0.2	114.73	17.76	6.27	3.07	1.79	1.16	0.81	0.60	0.46
	0.3	70.56	12.71	4.92	2.56	1.56	1.05	0.75	0.56	0.44
	0.4	49.68	10.24	4.23	2.29	1.43	0.98	0.71	0.54	0.42
	0.5	38.12	8.81	3.81	2.11	1.34	0.93	0.68	0.52	0.41
	0.6	31.23	7.90	3.53	1.99	1.27	0.88	0.65	0.50	0.39
	0.7	21.87	6.00	2.75	1.57	1.01	0.71	0.52	0.40	0.32
	0.8	19.30	5.57	2.59	1.49	0.96	0.67	0.50	0.38	0.30
	0.9	17.84	5.27	2.46	1.42	0.92	0.65	0.48	0.37	0.29
	1.0	17.16	5.05	2.36	1.36	0.88	0.62	0.46	0.35	0.28
0.6	0.1	323.56	42.99	13.40	5.88	3.09	1.80	1.12	0.73	0.48
	0.2	142.32	22.64	8.06	3.91	2.23	1.39	0.92	0.63	0.44
	0.3	84.89	16.05	6.28	3.24	1.92	1.23	0.83	0.58	0.41
	0.4	58.43	12.90	5.39	2.88	1.75	1.14	0.78	0.55	0.39
	0.5	44.34	11.13	4.86	2.66	1.63	1.07	0.74	0.52	0.37
	0.6	29.06	8.20	3.69	2.04	1.25	0.81	0.55	0.38	0.26
	0.7	24.71	7.51	3.44	1.91	1.18	0.77	0.52	0.35	0.24
	0.8	22.56	7.06	3.26	1.81	1.11	0.72	0.48	0.33	0.22
	0.9	21.89	6.78	3.12	1.73	1.06	0.68	0.45	0.30	0.20
	1.0	22.24	6.61	3.00	1.65	1.00	0.65	0.43	0.28	0.18
0.7	0.1	360.67	49.26	15.65	6.94	3.65	2.11	1.29	0.80	0.49
	0.2	152.32	25.82	9.48	4.66	2.65	1.63	1.04	0.68	0.44
	0.3	87.85	18.38	7.46	3.88	2.29	1.44	0.94	0.62	0.40
	0.4	59.34	14.92	6.47	3.48	2.09	1.33	0.87	0.58	0.37
	0.5	35.18	10.56	4.78	2.60	1.55	0.97	0.62	0.38	0.22
	0.6	28.26	9.51	4.41	2.42	1.45	0.90	0.57	0.35	0.19
	0.7	25.45	8.91	4.16	2.28	1.36	0.85	0.53	0.32	0.17
	0.8	25.21	8.60	3.99	2.18	1.29	0.79	0.49	0.28	0.14
	0.9	26.68	8.48	3.86	2.08	1.22	0.74	0.45	0.25	0.12
	1.0	29.34	8.49	3.77	2.01	1.16	0.70	0.41	0.22	0.10
0.8	0.1	343.46	49.71	16.47	7.52	4.02	2.35	1.43	0.87	0.51
	0.2	136.74	26.38	10.30	5.22	3.01	1.85	1.17	0.74	0.45
	0.3	75.52	19.20	8.32	4.45	2.64	1.66	1.06	0.67	0.41
	0.4	37.55	12.79	5.92	3.23	1.91	1.17	0.72	0.42	0.21
	0.5	27.25	11.28	5.41	2.98	1.77	1.08	0.66	0.37	0.18
	0.6	24.23	10.57	5.10	2.81	1.66	1.01	0.60	0.33	0.14
	0.7	25.36	10.32	4.91	2.69	1.57	0.94	0.55	0.29	0.11
	0.8	29.09	10.37	4.80	2.59	1.50	0.88	0.50	0.25	0.08
	0.9	34.55	10.60	4.74	2.50	1.42	0.82	0.46	0.21	0.05
	1.0	41.23	10.98	4.71	2.43	1.36	0.77	0.41	0.18	0.01
0.9	0.1	256.86	42.66	15.41	7.44	4.14	2.48	1.53	0.93	0.54
	0.2	90.70	23.73	10.34	5.54	3.28	2.05	1.30	0.81	0.47
	0.3	29.93	14.20	6.95	3.86	2.30	1.41	0.85	0.48	0.22
	0.4	16.27	12.21	6.28	3.55	2.12	1.29	0.77	0.42	0.18
	0.5	14.80	11.58	5.96	3.35	1.99	1.20	0.70	0.37	0.14
	0.6	19.43	11.62	5.81	3.23	1.89	1.13	0.64	0.32	0.10
	0.7	27.55	12.06	5.77	3.14	1.81	1.06	0.59	0.27	0.06
	0.8	37.84	12.73	5.79	3.07	1.74	0.99	0.53	0.23	0.02
	0.9	49.59	13.57	5.85	3.01	1.67	0.93	0.48	0.18	-0.02
	1.0	62.35	14.52	5.94	2.97	1.61	0.87	0.42	0.14	-0.06
1.0	0.1	94.95	27.29	12.24	6.64	3.96	2.48	1.57	0.98	0.57
	0.2	-6.40	12.70	7.32	4.31	2.64	1.64	1.00	0.56	0.25
	0.3	-17.35	10.90	6.66	3.97	2.44	1.51	0.90	0.49	0.20
	0.4	-11.05	11.02	6.50	3.82	2.32	1.41	0.83	0.43	0.15
	0.5	2.15	11.91	6.54	3.74	2.23	1.33	0.76	0.38	0.10
	0.6	18.80	13.18	6.67	3.70	2.16	1.26	0.70	0.32	0.06
	0.7	37.42	14.67	6.86	3.68	2.09	1.19	0.63	0.26	0.01
	0.8	57.27	16.30	7.09	3.67	2.03	1.12	0.57	0.21	-0.04
	0.9	77.95	18.02	7.35	3.66	1.97	1.06	0.51	0.15	-0.09
	1.0	99.20	19.80	7.61	3.67	1.92	1.00	0.45	0.10	-0.14

D5-3,  $D_c > 250$  mm, Converging

		$C_b$ Values								
		$Q_b/Q_c$								
$A_s/A_c$	$A_b/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1	0.1	-13.86	-1.90	0.03	0.61	0.83	0.92	0.96	0.98	0.98
	0.2	-58.25	-10.48	-2.80	-0.51	0.36	0.74	0.90	0.96	0.96
	0.3	-132.23	-24.75	-7.50	-2.36	-0.39	0.45	0.82	0.96	0.96
	0.4	-235.84	-44.74	-14.07	-4.93	-1.43	0.07	0.73	0.98	0.99
	0.5	-369.15	-70.45	-22.51	-8.23	-2.76	-0.42	0.61	1.01	1.05
	0.6	-532.21	-101.89	-32.83	-12.26	-4.38	-1.00	0.48	1.06	1.13
	0.7	-725.06	-139.08	-45.04	-17.02	-6.30	-1.70	0.33	1.13	1.24
	0.8	-947.77	-182.03	-59.15	-22.53	-8.52	-2.50	0.16	1.22	1.38
	0.9	-1200.	-230.76	-75.15	-28.78	-11.03	-3.40	-0.03	1.32	1.55
	1.0	-1483.	-285.27	-93.06	-35.78	-13.84	-4.41	-0.25	1.43	1.75
0.2	0.1	-5.86	-0.35	0.54	0.81	0.91	0.95	0.97	0.97	0.96
	0.2	-26.08	-4.19	-0.70	0.33	0.71	0.87	0.93	0.95	0.93
	0.3	-59.71	-10.53	-2.72	-0.43	0.43	0.78	0.91	0.95	0.91
	0.4	-106.78	-19.39	-5.53	-1.46	0.05	0.67	0.91	0.97	0.91
	0.5	-167.36	-30.77	-9.12	-2.78	-0.42	0.55	0.93	1.02	0.93
	0.6	-241.50	-44.68	-13.50	-4.37	-0.97	0.42	0.96	1.10	0.98
	0.7	-329.25	-61.15	-18.68	-6.25	-1.62	0.27	1.02	1.21	1.06
	0.8	-430.67	-80.18	-24.67	-8.42	-2.37	0.10	1.09	1.35	1.17
	0.9	-545.81	-101.78	-31.47	-10.89	-3.22	-0.08	1.17	1.52	1.31
	1.0	-674.72	-125.98	-39.08	-13.64	-4.17	-0.28	1.28	1.72	1.48
0.3	0.1	-3.26	0.15	0.70	0.86	0.93	0.96	0.97	0.97	0.95
	0.2	-15.50	-2.16	-0.04	0.58	0.81	0.90	0.93	0.94	0.91
	0.3	-35.76	-5.90	-1.20	0.16	0.66	0.85	0.92	0.92	0.88
	0.4	-64.09	-11.09	-2.78	-0.38	0.48	0.82	0.93	0.94	0.86
	0.5	-100.54	-17.73	-4.78	-1.06	0.29	0.80	0.97	0.98	0.87
	0.6	-145.16	-25.85	-7.21	-1.86	0.06	0.80	1.05	1.05	0.90
	0.7	-198.01	-35.46	-10.08	-2.81	-0.19	0.82	1.15	1.16	0.96
	0.8	-259.13	-46.56	-13.39	-3.89	-0.47	0.85	1.28	1.30	1.05
	0.9	-328.59	-59.18	-17.15	-5.11	-0.78	0.89	1.44	1.47	1.17
	1.0	-406.44	-73.33	-21.37	-6.48	-1.12	0.94	1.63	1.68	1.32
0.4	0.1	-1.99	0.38	0.77	0.89	0.94	0.96	0.97	0.97	0.95
	0.2	-10.31	-1.18	0.26	0.69	0.84	0.91	0.93	0.93	0.90
	0.3	-23.96	-3.65	-0.48	0.43	0.75	0.88	0.91	0.91	0.86
	0.4	-42.98	-7.03	-1.46	0.11	0.67	0.87	0.93	0.91	0.84
	0.5	-67.44	-11.35	-2.69	-0.26	0.59	0.90	0.97	0.94	0.84
	0.6	-97.39	-16.60	-4.17	-0.69	0.52	0.95	1.06	1.01	0.87
	0.7	-132.88	-22.81	-5.91	-1.17	0.46	1.03	1.17	1.11	0.92
	0.8	-173.96	-29.99	-7.90	-1.73	0.40	1.15	1.33	1.24	1.00
	0.9	-220.69	-38.15	-10.16	-2.35	0.35	1.29	1.51	1.40	1.11
	1.0	-273.12	-47.31	-12.70	-3.04	0.29	1.45	1.74	1.61	1.26
0.5	0.1	-1.26	0.51	0.81	0.90	0.94	0.96	0.97	0.96	0.95
	0.2	-7.26	-0.62	0.43	0.75	0.86	0.91	0.93	0.93	0.90
	0.3	-16.99	-2.35	-0.07	0.57	0.80	0.89	0.91	0.90	0.87
	0.4	-30.49	-4.67	-0.72	0.38	0.76	0.89	0.92	0.90	0.85
	0.5	-47.82	-7.61	-1.50	0.19	0.75	0.93	0.97	0.93	0.85
	0.6	-69.03	-11.17	-2.42	-0.03	0.76	1.01	1.05	0.98	0.88
	0.7	-94.17	-15.37	-3.49	-0.26	0.80	1.13	1.17	1.07	0.93
	0.8	-123.30	-20.22	-4.71	-0.50	0.87	1.29	1.33	1.20	1.02
	0.9	-156.48	-25.73	-6.09	-0.77	0.96	1.48	1.53	1.36	1.13
	1.0	-193.74	-31.92	-7.63	-1.07	1.06	1.71	1.77	1.56	1.28
0.6	0.1	-0.79	0.59	0.83	0.91	0.95	0.96	0.97	0.97	0.95
	0.2	-5.28	-0.27	0.54	0.78	0.88	0.91	0.93	0.93	0.91
	0.3	-12.43	-1.51	0.18	0.66	0.83	0.89	0.91	0.91	0.89
	0.4	-22.29	-3.15	-0.25	0.55	0.82	0.90	0.92	0.91	0.88
	0.5	-34.92	-5.19	-0.74	0.46	0.84	0.95	0.96	0.93	0.89
	0.6	-50.35	-7.64	-1.30	0.38	0.91	1.05	1.04	0.98	0.93
	0.7	-68.66	-10.52	-1.94	0.32	1.01	1.18	1.16	1.07	0.99
	0.8	-89.89	-13.83	-2.65	0.26	1.15	1.36	1.33	1.19	1.08
	0.9	-114.09	-17.61	-3.46	0.22	1.32	1.59	1.53	1.35	1.21
	1.0	-141.33	-21.84	-4.35	0.18	1.54	1.85	1.77	1.54	1.37

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D5-3,  $D_c > 250$  mm, Converging (Continued)

		$C_b$ Values (Continued)								
		$Q_b/Q_c$								
$A_s/A_c$	$A_b/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.7	0.1	-0.47	0.65	0.85	0.92	0.95	0.96	0.97	0.97	0.96
	0.2	-3.90	-0.03	0.61	0.81	0.89	0.92	0.94	0.94	0.93
	0.3	-9.25	-0.94	0.35	0.72	0.85	0.90	0.92	0.92	0.92
	0.4	-16.54	-2.10	0.07	0.66	0.85	0.91	0.93	0.92	0.92
	0.5	-25.85	-3.51	-0.22	0.64	0.90	0.97	0.97	0.94	0.95
	0.6	-37.21	-5.18	-0.54	0.65	1.00	1.07	1.05	1.00	1.00
	0.7	-50.68	-7.13	-0.87	0.70	1.14	1.22	1.17	1.08	1.08
	0.8	-66.31	-9.37	-1.24	0.78	1.33	1.41	1.33	1.21	1.20
	0.9	-84.17	-11.92	-1.64	0.89	1.56	1.65	1.53	1.36	1.34
	1.0	-104.29	-14.78	-2.09	1.03	1.84	1.94	1.78	1.56	1.52
0.8	0.1	-0.23	0.69	0.87	0.93	0.95	0.97	0.97	0.98	0.97
	0.2	-2.90	0.15	0.67	0.83	0.90	0.93	0.94	0.95	0.96
	0.3	-6.91	-0.53	0.47	0.76	0.87	0.91	0.93	0.94	0.96
	0.4	-12.31	-1.34	0.30	0.74	0.88	0.93	0.94	0.95	0.98
	0.5	-19.16	-2.29	0.15	0.77	0.94	0.99	0.98	0.98	1.03
	0.6	-27.50	-3.39	0.01	0.84	1.06	1.09	1.06	1.03	1.11
	0.7	-37.38	-4.66	-0.11	0.97	1.23	1.24	1.18	1.12	1.21
	0.8	-48.87	-6.11	-0.22	1.15	1.46	1.45	1.35	1.25	1.35
	0.9	-62.01	-7.75	-0.33	1.37	1.73	1.70	1.55	1.41	1.52
	1.0	-76.85	-9.59	-0.44	1.63	2.06	2.00	1.80	1.61	1.73
0.9	0.1	-0.05	0.72	0.88	0.93	0.96	0.97	0.98	0.99	0.99
	0.2	-2.14	0.28	0.71	0.85	0.91	0.94	0.96	0.97	0.99
	0.3	-5.14	-0.21	0.57	0.80	0.88	0.92	0.95	0.97	1.02
	0.4	-9.09	-0.76	0.47	0.80	0.91	0.94	0.96	0.98	1.06
	0.5	-14.06	-1.36	0.42	0.86	0.98	1.01	1.01	1.02	1.14
	0.6	-20.08	-2.04	0.42	0.99	1.11	1.12	1.09	1.09	1.24
	0.7	-27.21	-2.79	0.47	1.17	1.30	1.27	1.21	1.19	1.38
	0.8	-35.50	-3.63	0.55	1.42	1.55	1.49	1.38	1.32	1.55
	0.9	-45.01	-4.57	0.66	1.72	1.86	1.75	1.59	1.49	1.75
	1.0	-55.79	-5.64	0.80	2.08	2.22	2.06	1.84	1.69	1.99
1.0	0.1	0.09	0.75	0.89	0.94	0.97	0.98	0.99	1.00	1.01
	0.2	-1.54	0.39	0.74	0.87	0.92	0.95	0.97	0.99	1.03
	0.3	-3.75	0.03	0.64	0.83	0.90	0.94	0.97	1.00	1.08
	0.4	-6.57	-0.32	0.61	0.85	0.93	0.97	0.99	1.03	1.16
	0.5	-10.05	-0.65	0.64	0.94	1.02	1.03	1.04	1.08	1.26
	0.6	-14.24	-0.98	0.74	1.10	1.16	1.15	1.13	1.16	1.40
	0.7	-19.20	-1.32	0.91	1.33	1.37	1.31	1.26	1.27	1.57
	0.8	-24.98	-1.69	1.14	1.63	1.63	1.53	1.43	1.41	1.78
	0.9	-31.62	-2.10	1.42	2.00	1.96	1.80	1.64	1.59	2.02
	1.0	-39.19	-2.55	1.76	2.43	2.35	2.12	1.90	1.81	2.30

		$C_s$ Values								
		$Q_b/Q_c$								
$A_s/A_c$	$A_b/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1	0.1	7.87	1.70	1.07	0.92	0.86	0.84	0.82	0.82	0.81
	0.2	4.21	1.30	0.97	0.88	0.85	0.83	0.82	0.81	0.81
	0.3	3.02	1.16	0.93	0.87	0.84	0.83	0.82	0.81	0.81
	0.4	2.45	1.10	0.92	0.86	0.84	0.83	0.82	0.81	0.81
	0.5	2.13	1.07	0.91	0.86	0.84	0.82	0.82	0.81	0.81
	0.6	1.93	1.04	0.90	0.86	0.84	0.82	0.82	0.81	0.81
	0.7	1.80	1.03	0.90	0.85	0.83	0.82	0.82	0.81	0.81
	0.8	1.72	1.02	0.90	0.85	0.83	0.82	0.82	0.81	0.81
	0.9	1.67	1.01	0.89	0.85	0.83	0.82	0.82	0.81	0.81
	1.0	1.63	1.01	0.89	0.85	0.83	0.82	0.82	0.81	0.81
0.2	0.1	44.93	6.00	2.16	1.24	0.92	0.78	0.71	0.67	0.65
	0.2	20.43	3.28	1.45	0.98	0.81	0.73	0.69	0.66	0.64
	0.3	12.53	2.40	1.22	0.90	0.77	0.71	0.68	0.66	0.64
	0.4	8.78	1.98	1.12	0.86	0.76	0.70	0.67	0.66	0.64
	0.5	6.69	1.75	1.06	0.84	0.75	0.70	0.67	0.65	0.64
	0.6	5.43	1.61	1.02	0.83	0.74	0.70	0.67	0.65	0.64
	0.7	4.64	1.52	1.00	0.82	0.74	0.70	0.67	0.65	0.64
	0.8	4.15	1.47	0.98	0.81	0.74	0.69	0.67	0.65	0.64
	0.9	3.86	1.43	0.97	0.81	0.74	0.69	0.67	0.65	0.64
	1.0	3.71	1.42	0.97	0.81	0.73	0.69	0.67	0.65	0.64

D5-3,  $D_c > 250$  mm, Converging (Continued)

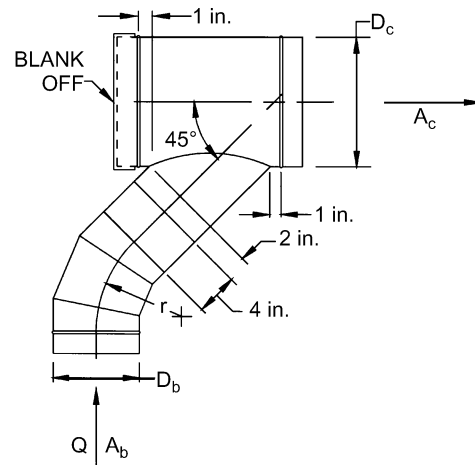
		$C_s$ Values (Continued)								
		$Q_b/Q_c$								
$A_s/A_c$	$A_b/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.3	0.1	118.96	14.64	4.45	2.03	1.20	0.84	0.66	0.57	0.51
	0.2	51.24	7.11	2.49	1.33	0.90	0.70	0.60	0.54	0.50
	0.3	29.57	4.70	1.87	1.10	0.80	0.66	0.58	0.53	0.50
	0.4	19.40	3.57	1.58	1.00	0.76	0.64	0.57	0.52	0.50
	0.5	13.84	2.96	1.42	0.94	0.73	0.62	0.56	0.52	0.50
	0.6	10.58	2.59	1.32	0.90	0.72	0.62	0.56	0.52	0.49
	0.7	8.64	2.38	1.27	0.88	0.71	0.61	0.56	0.52	0.49
	0.8	7.52	2.25	1.23	0.87	0.70	0.61	0.56	0.52	0.49
	0.9	6.95	2.19	1.22	0.87	0.70	0.61	0.56	0.52	0.49
	1.0	6.76	2.17	1.21	0.86	0.70	0.61	0.55	0.52	0.49
0.4	0.1	218.57	26.35	7.61	3.18	1.65	1.00	0.68	0.50	0.40
	0.2	90.30	12.10	3.91	1.85	1.08	0.74	0.55	0.45	0.38
	0.3	49.68	7.59	2.74	1.42	0.90	0.65	0.51	0.43	0.37
	0.4	30.96	5.51	2.21	1.23	0.82	0.61	0.49	0.42	0.37
	0.5	21.00	4.40	1.92	1.13	0.78	0.59	0.48	0.42	0.37
	0.6	15.43	3.78	1.76	1.07	0.75	0.58	0.48	0.41	0.37
	0.7	12.36	3.44	1.67	1.04	0.74	0.57	0.48	0.41	0.37
	0.8	10.86	3.27	1.63	1.02	0.73	0.57	0.47	0.41	0.37
	0.9	10.40	3.22	1.61	1.01	0.73	0.57	0.47	0.41	0.37
	1.0	10.67	3.25	1.62	1.02	0.73	0.57	0.47	0.41	0.37
0.5	0.1	320.10	38.52	10.97	4.44	2.18	1.21	0.72	0.46	0.31
	0.2	126.36	16.99	5.39	2.42	1.32	0.81	0.54	0.38	0.28
	0.3	65.94	10.28	3.65	1.79	1.05	0.68	0.48	0.35	0.27
	0.4	38.84	7.27	2.87	1.51	0.93	0.63	0.45	0.34	0.27
	0.5	25.07	5.74	2.47	1.37	0.87	0.60	0.44	0.33	0.26
	0.6	17.98	4.95	2.27	1.29	0.84	0.58	0.43	0.33	0.26
	0.7	14.69	4.58	2.17	1.26	0.82	0.58	0.43	0.33	0.26
	0.8	13.78	4.48	2.15	1.25	0.82	0.57	0.43	0.33	0.26
	0.9	14.45	4.56	2.17	1.26	0.82	0.58	0.43	0.33	0.26
	1.0	16.24	4.76	2.22	1.28	0.83	0.58	0.43	0.33	0.26
0.6	0.1	393.66	47.81	13.66	5.50	2.64	1.40	0.78	0.44	0.23
	0.2	146.22	20.32	6.54	2.92	1.54	0.89	0.54	0.33	0.20
	0.3	70.93	11.95	4.37	2.13	1.20	0.73	0.46	0.30	0.18
	0.4	38.66	8.37	3.44	1.80	1.06	0.67	0.43	0.28	0.18
	0.5	23.61	6.70	3.00	1.64	0.99	0.64	0.42	0.28	0.18
	0.6	17.17	5.98	2.82	1.57	0.97	0.62	0.41	0.27	0.18
	0.7	15.64	5.81	2.77	1.56	0.96	0.62	0.41	0.27	0.18
	0.8	17.19	5.98	2.82	1.57	0.97	0.62	0.41	0.27	0.18
	0.9	20.79	6.38	2.92	1.61	0.98	0.63	0.42	0.27	0.18
	1.0	25.82	6.94	3.07	1.66	1.00	0.64	0.42	0.28	0.18
0.7	0.1	409.10	50.88	14.82	6.03	2.90	1.51	0.81	0.41	0.17
	0.2	137.78	20.74	7.01	3.21	1.70	0.96	0.54	0.29	0.13
	0.3	58.74	11.96	4.73	2.39	1.34	0.79	0.47	0.26	0.12
	0.4	27.78	8.52	3.84	2.06	1.21	0.73	0.44	0.24	0.11
	0.5	16.04	7.21	3.50	1.94	1.15	0.71	0.43	0.24	0.11
	0.6	13.91	6.97	3.44	1.92	1.14	0.70	0.42	0.24	0.11
	0.7	17.28	7.35	3.54	1.95	1.16	0.71	0.43	0.24	0.11
	0.8	24.08	8.10	3.73	2.02	1.19	0.72	0.43	0.24	0.11
	0.9	33.17	9.11	3.99	2.12	1.23	0.74	0.44	0.25	0.11
	1.0	43.86	10.30	4.30	2.23	1.28	0.76	0.45	0.25	0.11
0.8	0.1	341.98	45.02	13.75	5.80	2.86	1.50	0.79	0.38	0.12
	0.2	92.97	17.35	6.57	3.21	1.75	0.99	0.55	0.27	0.08
	0.3	26.98	10.02	4.67	2.52	1.46	0.86	0.48	0.24	0.07
	0.4	6.75	7.77	4.09	2.31	1.37	0.81	0.46	0.23	0.06
	0.5	4.83	7.56	4.03	2.29	1.36	0.81	0.46	0.23	0.06
	0.6	12.05	8.36	4.24	2.37	1.39	0.83	0.47	0.23	0.07
	0.7	24.51	9.75	4.60	2.49	1.45	0.85	0.48	0.24	0.07
	0.8	40.23	11.49	5.05	2.66	1.52	0.88	0.50	0.24	0.07
	0.9	58.13	13.48	5.57	2.85	1.60	0.92	0.51	0.25	0.07
	1.0	77.56	15.64	6.13	3.05	1.68	0.96	0.53	0.26	0.08

D5-3,  $D_c > 250$  mm, Converging (Continued)

		$C_s$ Values (Concluded)								
		$Q_b/Q_c$								
$A_s/A_c$	$A_b/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.9	0.1	179.59	28.81	10.06	4.66	2.45	1.34	0.71	0.32	0.07
	0.2	10.77	10.05	5.20	2.91	1.70	0.99	0.55	0.25	0.04
	0.3	-21.27	6.49	4.28	2.57	1.56	0.93	0.52	0.24	0.04
	0.4	-19.11	6.73	4.34	2.60	1.57	0.93	0.52	0.24	0.04
	0.5	-3.28	8.49	4.80	2.76	1.64	0.97	0.54	0.24	0.04
	0.6	19.39	11.01	5.45	3.00	1.74	1.01	0.56	0.25	0.04
	0.7	45.97	13.96	6.21	3.27	1.86	1.07	0.58	0.27	0.05
	0.8	74.99	17.18	7.05	3.58	1.98	1.13	0.61	0.28	0.05
	0.9	105.64	20.59	7.93	3.89	2.12	1.19	0.64	0.29	0.06
1.0	1.0	137.43	24.12	8.85	4.23	2.26	1.26	0.67	0.31	0.06
	0.1	-73.14	2.79	3.92	2.68	1.70	1.04	0.58	0.26	0.03
	0.2	-99.78	-0.17	3.15	2.40	1.58	0.98	0.56	0.25	0.02
	0.3	-75.42	2.54	3.85	2.65	1.69	1.03	0.58	0.26	0.03
	0.4	-38.31	6.66	4.92	3.04	1.86	1.11	0.62	0.28	0.03
	0.5	3.90	11.35	6.14	3.48	2.04	1.20	0.66	0.29	0.04
	0.6	48.66	16.32	7.43	3.94	2.24	1.29	0.70	0.31	0.04
	0.7	94.88	21.46	8.76	4.43	2.45	1.38	0.75	0.33	0.05
	0.8	142.01	26.70	10.12	4.92	2.66	1.48	0.79	0.35	0.06
0.9	189.74	32.00	11.49	5.41	2.87	1.58	0.84	0.37	0.07	
1.0	237.90	37.35	12.88	5.92	3.08	1.68	0.88	0.39	0.07	

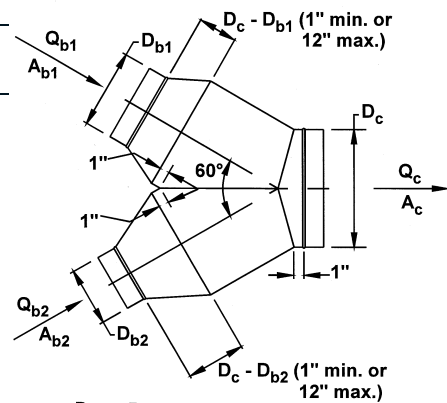
ED5-6 Capped Wye, Branch with 45-Degree Elbow, Branch 90 Degrees to Main, Converging,  $r/D_b = 1.5$

$A_b/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
$C_b$	1.02	0.97	0.93	0.88	0.84	0.79	0.75	0.70	0.66	0.61



ED5-9 Symmetrical Wye, 60 Degree,  $D_{b1} \geq D_{b2}$ , Converging

		$C_{b1}$ Values								
		$Q_{b1}/Q_c$								
$A_{b1}/A_c$	$A_{b2}/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1	0.1	-3.00	-0.50	-0.11	0.06	0.12	0.14	0.14	0.13	0.11
	0.2	-16.00	-3.00	-1.01	0.01	0.32	0.44	0.49	0.56	0.49
0.2	0.2	-11.95	-1.89	-0.09	0.41	0.62	0.74	0.80	0.80	0.79
	0.3	-54.00	-11.25	-3.57	-0.43	-0.22	0.38	0.55	1.41	1.22
0.3	0.2	-45.45	-9.39	-2.44	-0.41	0.33	0.68	0.89	1.03	1.13
	0.3	-16.88	-2.92	-0.09	0.59	0.85	1.02	1.12	1.12	1.22
0.4	0.1	-97.28	-18.48	-6.35	-1.58	-0.57	-0.15	0.23	0.35	0.50
	0.2	-72.04	-14.00	-4.26	-1.24	-0.32	0.09	0.40	0.50	0.62
0.3	0.3	-52.95	-9.91	-2.86	-0.91	-0.06	0.32	0.56	0.64	0.73
	0.4	-40.00	-6.22	-2.15	-0.57	0.19	0.56	0.72	0.79	0.85
0.5	0.1	-167.71	-32.20	-10.05	-2.52	-1.25	-0.26	0.17	0.34	0.36
	0.2	-126.04	-23.80	-7.44	-2.64	-0.85	-0.13	0.16	0.26	0.28
0.3	0.3	-91.07	-16.91	-5.16	-1.73	-0.46	0.04	0.23	0.29	0.28
	0.4	-56.41	-10.07	-2.90	-0.82	-0.07	0.21	0.30	0.31	0.29
0.5	0.5	-30.58	-5.23	-1.06	0.00	0.32	0.43	0.47	0.47	0.41



ED5-9 Symmetrical Wye, 60 Degree,  $D_{b1} \geq D_{b2}$ , Converging (Continued)

		$C_{b1}$ Values (Concluded)									
		$Q_{b1}/Q_c$									
$A_{b1}/A_c$	$A_{b2}/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	
0.6	0.1	-299.02	-55.99	-16.77	-5.89	-2.09	-0.54	0.11	0.25	0.23	
	0.2	-209.81	-39.31	-12.13	-4.35	-1.54	-0.40	0.06	0.25	0.23	
	0.3	-147.43	-27.69	-8.75	-3.20	-1.13	-0.29	0.07	0.23	0.22	
	0.4	-85.06	-16.07	-5.38	-2.04	-0.71	-0.17	0.08	0.23	0.22	
	0.5	-58.22	-11.03	-3.84	-1.49	-0.50	-0.09	0.11	0.23	0.22	
	0.6	-40.57	-7.86	-2.60	-0.99	-0.32	0.00	0.14	0.23	0.22	
0.7	0.1	-420.02	-77.23	-23.37	-8.01	-3.30	-1.46	-0.71	-0.10	0.03	
	0.2	-285.70	-53.45	-16.65	-6.05	-2.52	-1.02	-0.46	-0.02	0.06	
	0.3	-195.01	-37.35	-12.21	-4.72	-1.87	-0.77	-0.14	0.04	0.09	
	0.4	-104.16	-21.18	-7.20	-3.23	-1.37	-0.39	-0.10	0.08	0.12	
	0.5	-67.21	-13.02	-4.52	-1.78	-0.73	-0.26	-0.03	0.12	0.15	
	0.6	-49.01	-9.63	-3.13	-1.28	-0.51	-0.14	-0.02	0.16	0.17	
	0.7	-59.33	-10.05	-2.53	-0.54	-0.21	-0.09	-0.01	0.23	0.24	
0.8	0.1	-518.26	-95.93	-30.34	-11.09	-4.30	-2.51	-1.58	-0.63	-0.31	
	0.2	-373.33	-69.73	-21.93	-8.08	-3.84	-1.96	-1.31	-0.50	-0.24	
	0.3	-247.31	-48.35	-16.32	-6.65	-2.89	-1.51	-0.49	-0.30	-0.16	
	0.4	-120.88	-26.76	-9.24	-4.80	-2.30	-0.71	-0.39	-0.20	-0.08	
	0.5	-72.08	-14.20	-4.98	-2.00	-1.02	-0.53	-0.26	-0.10	0.01	
	0.6	-55.91	-11.20	-3.56	-1.60	-0.77	-0.36	-0.13	0.01	0.05	
	0.7	-35.96	-7.20	-2.31	-1.08	-0.45	-0.09	0.03	0.11	0.13	
	0.8	-16.00	-3.20	-1.07	-0.56	-0.13	0.18	0.20	0.20	0.21	
0.9	0.1	-629.39	-114.67	-35.12	-13.73	-6.55	-3.65	-2.25	-1.20	-0.70	
	0.2	-473.23	-88.43	-27.99	-11.44	-5.67	-3.21	-2.07	-1.11	-0.65	
	0.3	-303.64	-60.65	-21.13	-9.65	-4.91	-2.87	-1.51	-0.95	-0.58	
	0.4	-216.44	-44.78	-16.20	-8.35	-4.46	-2.31	-1.43	-0.87	-0.52	
	0.5	-116.49	-28.35	-12.15	-6.45	-3.65	-2.19	-1.35	-0.81	-0.47	
	0.6	-98.16	-25.31	-10.76	-5.82	-3.48	-2.16	-1.35	-0.81	-0.49	
	0.7	-78.15	-21.31	-9.54	-5.37	-3.28	-1.99	-1.25	-0.75	-0.44	
	0.8	-58.15	-17.32	-8.33	-4.93	-3.08	-1.82	-1.15	-0.69	-0.39	
	0.9	-72.90	-18.23	-8.10	-4.56	-2.92	-1.92	-1.29	-0.66	-0.39	
1.0	0.1	-677.01	-124.30	-37.45	-16.24	-8.10	-4.89	-3.06	-1.95	-1.23	
	0.2	-585.16	-109.39	-34.85	-15.63	-8.00	-4.86	-3.06	-1.95	-1.23	
	0.3	-363.31	-74.20	-26.68	-13.44	-7.60	-4.72	-2.96	-1.88	-1.17	
	0.4	-345.54	-68.75	-25.56	-13.13	-7.40	-4.58	-2.92	-1.84	-1.16	
	0.5	-175.00	-47.50	-22.22	-12.81	-7.40	-4.58	-2.92	-1.84	-1.16	
	0.6	-155.00	-45.00	-21.00	-11.88	-7.40	-4.77	-3.13	-2.02	-1.28	
	0.7	-136.79	-41.38	-19.95	-11.58	-7.40	-4.77	-3.13	-2.02	-1.28	
	0.8	-118.58	-37.76	-18.91	-11.29	-7.40	-4.77	-3.13	-2.02	-1.28	
	0.9	-100.29	-34.13	-17.90	-10.99	-7.39	-4.77	-3.13	-2.02	-1.28	
	1.0	-82.00	-30.50	-16.89	-10.69	-7.39	-4.77	-3.13	-2.02	-1.28	

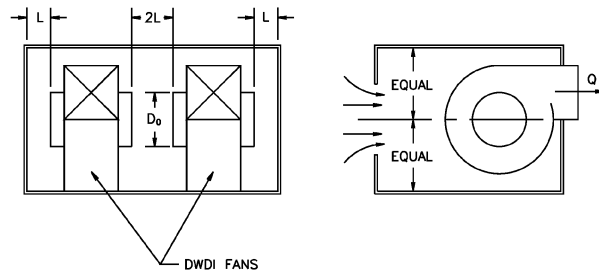
		$C_{b1}$ Values									
		$Q_{b2}/Q_c$									
$A_{b1}/A_c$	$A_{b2}/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	
0.1	0.1	-3.00	-0.50	-0.11	0.06	0.12	0.14	0.14	0.13	0.11	
0.2	0.1	-2.70	-0.04	0.23	0.15	0.16	0.18	0.20	0.17	0.16	
	0.2	-11.95	-1.89	-0.09	0.41	0.62	0.74	0.80	0.80	0.79	
0.3	0.1	-2.12	0.12	0.33	0.22	0.22	0.23	0.26	0.22	0.22	
	0.2	-2.00	-0.30	0.22	0.42	0.61	0.73	0.78	0.77	0.76	
	0.3	-16.88	-2.92	-0.09	0.59	0.85	1.02	1.12	1.12	1.22	
0.4	0.1	-2.38	-0.17	0.13	0.23	0.25	0.24	0.23	0.24	0.24	
	0.2	-6.95	-1.00	0.16	0.53	0.67	0.71	0.72	0.72	0.71	
	0.3	-16.21	-2.90	-0.44	0.40	0.79	0.98	1.05	1.06	1.05	
	0.4	-40.00	-6.22	-2.15	-0.57	0.19	0.56	0.72	0.79	0.85	
0.5	0.1	-1.58	0.11	0.33	0.31	0.32	0.33	0.34	0.32	0.32	
	0.2	-4.82	-0.01	0.56	0.71	0.82	0.89	0.92	0.90	0.89	
	0.3	-12.27	-1.17	0.44	0.88	1.11	1.25	1.29	1.25	1.23	
	0.4	-22.40	-2.93	-0.21	0.48	0.73	0.84	0.88	0.87	0.82	
	0.5	-30.58	-5.23	-1.06	0.00	0.32	0.43	0.47	0.46	0.41	

ED5-9 Symmetrical Wye, 60 Degree,  $D_{b1} \geq D_{b2}$ , Converging (Continued)

		$C_{b1}$ Values (Concluded)								
		$Q_{b2}/Q_c$								
$A_{b1}/A_c$	$A_{b2}/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.6	0.1	-0.78	0.11	0.32	0.40	0.42	0.43	0.43	0.42	0.42
	0.2	-3.68	0.07	0.77	0.98	1.06	1.08	1.08	1.06	1.04
	0.3	-9.06	-0.55	0.86	1.27	1.42	1.48	1.49	1.46	1.42
	0.4	-17.62	-2.12	0.06	0.60	0.83	0.95	0.98	0.95	0.91
	0.5	-28.00	-4.26	-0.99	-0.16	0.20	0.39	0.45	0.41	0.38
	0.6	-40.57	-7.86	-2.60	-0.99	-0.32	0.00	0.14	0.23	0.22
0.7	0.1	-0.12	0.17	0.22	0.34	0.39	0.40	0.40	0.39	0.39
	0.2	-1.24	0.33	0.55	0.86	0.98	1.02	1.04	1.03	1.02
	0.3	-4.03	0.06	0.73	1.20	1.39	1.47	1.49	1.47	1.44
	0.4	-9.77	-0.84	0.30	0.36	0.71	0.89	0.97	0.98	0.97
	0.5	-15.88	-2.51	-0.34	-0.06	0.21	0.51	0.65	0.68	0.70
	0.6	-23.89	-4.60	-1.54	-0.55	-0.51	-0.04	0.21	0.37	0.44
	0.7	-59.33	-10.05	-2.53	-0.54	-0.21	-0.09	-0.01	0.23	0.24
0.8	0.1	0.53	0.24	0.12	0.29	0.36	0.37	0.37	0.36	0.35
	0.2	1.20	0.60	0.33	0.73	0.90	0.97	1.00	1.00	0.99
	0.3	0.99	0.68	0.60	1.13	1.36	1.45	1.49	1.48	1.46
	0.4	-1.92	0.44	0.53	0.11	0.59	0.83	0.96	1.01	1.03
	0.5	-3.75	-0.75	0.31	0.05	0.22	0.62	0.84	0.96	1.03
	0.6	-7.20	-1.35	-0.48	-0.11	-0.70	-0.09	0.28	0.51	0.65
	0.7	-11.03	-2.14	-0.74	-0.29	-2.11	0.01	0.26	0.42	0.52
	0.8	-16.00	-3.20	-1.07	-0.56	-0.13	0.18	0.20	0.20	0.21
0.9	0.1	-0.13	0.32	0.23	0.32	0.36	0.36	0.36	0.35	0.34
	0.2	-0.98	0.80	0.61	0.85	0.97	1.03	1.04	1.03	1.01
	0.3	-3.06	0.35	0.55	1.06	1.32	1.44	1.49	1.49	1.48
	0.4	-7.36	-2.06	-1.01	-0.12	0.47	0.78	0.95	1.04	1.09
	0.5	-11.88	-4.00	-1.88	-0.98	-0.30	0.24	0.56	0.75	0.87
	0.6	-18.18	-5.99	-3.20	-1.67	-1.08	-0.30	0.18	0.49	0.70
	0.7	-25.36	-8.36	-4.42	-2.45	-2.82	-0.55	-0.01	0.34	0.56
	0.8	-33.92	-11.20	-5.87	-3.43	-1.94	-0.90	-0.35	0.00	0.24
	0.9	-72.90	-18.23	-8.10	-4.56	-2.92	-1.92	-1.29	-0.66	-0.39
1.0	0.1	-0.78	0.40	0.33	0.35	0.36	0.36	0.35	0.34	0.33
	0.2	-3.16	1.00	0.89	0.96	1.05	1.08	1.08	1.06	1.04
	0.3	-7.11	0.02	0.50	0.99	1.29	1.43	1.49	1.50	1.50
	0.4	-12.80	-4.56	-2.56	-0.36	0.35	0.72	0.93	1.07	1.15
	0.5	-20.00	-7.25	-4.06	-2.02	-0.81	-0.14	0.27	0.54	0.72
	0.6	-29.16	-10.62	-5.92	-3.24	-1.47	-0.50	0.09	0.48	0.74
	0.7	-39.69	-14.58	-8.11	-4.61	-3.53	-1.10	-0.28	0.25	0.60
	0.8	-51.84	-19.20	-10.67	-6.30	-3.75	-1.97	-0.89	-0.20	0.27
	0.9	-66.02	-24.50	-13.59	-8.31	-5.93	-3.18	-1.83	-0.95	-0.35
	1.0	-82.00	-30.50	-16.89	-10.69	-7.39	-4.77	-3.13	-2.02	-1.28

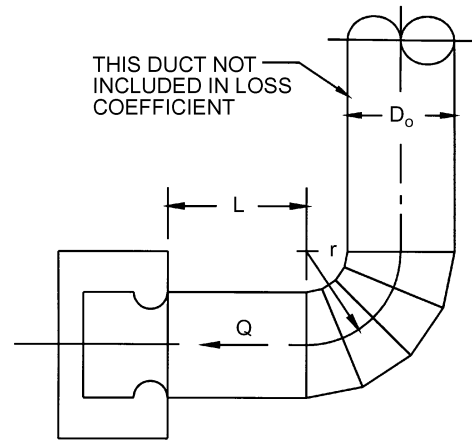
ED7-1 Centrifugal Fan Located in Plenum or Cabinet

$L/D_o$	0.30	0.40	0.50	0.75
$C_o$	0.80	0.53	0.40	0.22



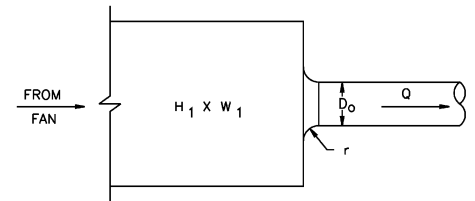
**ED7-2 Fan Inlet, Centrifugal, SWSI, with 4 Gore Elbow**

$r/D_o$	$C_o$ Values			
	0.0	2.0	5.0	10.0
0.50	1.80	1.00	0.53	0.53
0.75	1.40	0.80	0.40	0.40
1.00	1.20	0.67	0.33	0.33
1.50	1.10	0.60	0.33	0.33
2.00	1.00	0.53	0.33	0.33
3.00	0.67	0.40	0.22	0.22



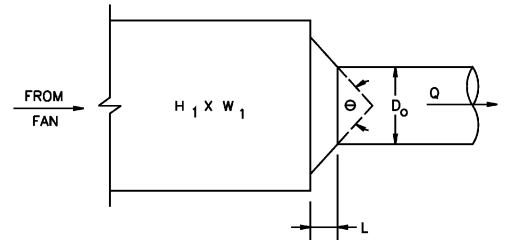
**SD1-1 Bellmouth, Plenum to Round, Supply Air Systems**

$r/D_o$	0.0	0.01	0.02	0.03	0.04	0.05	0.06	0.08	0.10	0.12	0.16	0.20	10.0
$C_o$	0.50	0.44	0.37	0.31	0.26	0.22	0.20	0.15	0.12	0.09	0.06	0.03	0.03



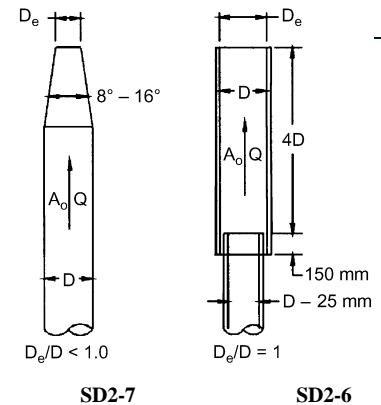
**SD1-2 Conical Bellmouth/Sudden Contraction, Plenum to Round, Supply Air Systems**

$L/D_o$	$C_o$ Values									
	0	10	20	30	45	60	100	140	180	
0.00	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
0.025	0.50	0.47	0.45	0.43	0.41	0.40	0.42	0.45	0.50	0.50
0.05	0.50	0.45	0.41	0.36	0.33	0.30	0.35	0.42	0.50	0.50
0.075	0.50	0.42	0.35	0.30	0.26	0.23	0.30	0.40	0.50	0.50
0.10	0.50	0.39	0.32	0.25	0.22	0.18	0.27	0.38	0.50	0.50
0.15	0.50	0.37	0.27	0.20	0.16	0.15	0.25	0.37	0.50	0.50
0.60	0.50	0.27	0.18	0.13	0.11	0.12	0.23	0.36	0.50	0.50

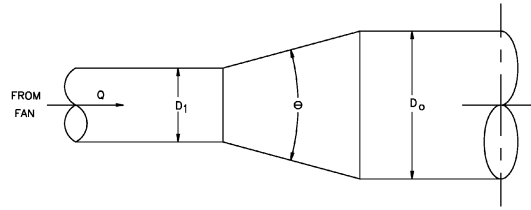


**SD2-6 and SD2-7 Stackheads**

$D_e/D$	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
$C_o$	130.	41.02	16.80	8.10	4.37	2.56	1.60	1.00



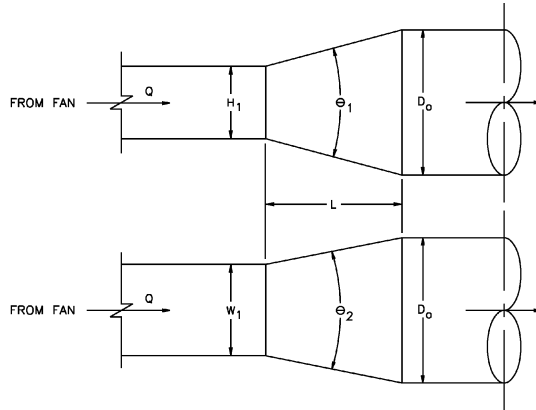
SD4-1 Transition, Round to Round, Supply Air Systems



$C_o$  Values

$A_o/A_1$	$\theta$												
	0	3	5	10	15	20	30	45	60	90	120	150	180
0.10	0.0	0.12	0.09	0.05	0.05	0.05	0.05	0.06	0.08	0.19	0.29	0.37	0.43
0.167	0.0	0.11	0.08	0.05	0.04	0.04	0.04	0.06	0.07	0.18	0.28	0.36	0.42
0.25	0.0	0.10	0.07	0.05	0.04	0.04	0.04	0.06	0.07	0.17	0.27	0.35	0.41
0.39	0.0	0.10	0.07	0.05	0.05	0.05	0.05	0.06	0.06	0.16	0.25	0.32	0.36
0.50	0.0	0.07	0.06	0.05	0.05	0.05	0.05	0.06	0.07	0.13	0.18	0.23	0.24
0.64	0.0	0.07	0.07	0.05	0.04	0.04	0.04	0.05	0.06	0.09	0.13	0.17	0.19
1.0	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.0	0.0	0.59	0.51	0.43	0.52	0.76	1.26	1.32	1.30	1.26	1.23	1.21	1.19
4.0	0.0	3.15	2.78	2.51	3.38	4.77	7.38	9.70	10.88	10.29	10.08	9.96	9.84
6.0	0.0	6.55	6.08	6.44	9.14	11.92	17.35	23.58	27.58	26.71	26.32	26.15	25.99
10.0	0.0	19.50	18.25	20.00	27.30	38.00	58.50	76.00	80.00	83.40	84.00	83.35	82.70
16.0	0.0	45.82	44.80	50.18	73.73	96.77	153.60	215.04	225.28	225.28	225.28	225.28	225.28

SD4-2 Transition, Rectangular to Round, Supply Air Systems



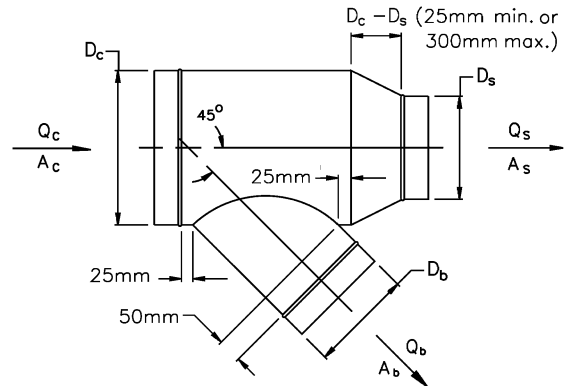
$C_o$  Values

$A_o/A_1$	$\theta$												
	0	3	5	10	15	20	30	45	60	90	120	150	180
0.10	0.0	0.12	0.09	0.05	0.05	0.05	0.05	0.06	0.08	0.19	0.29	0.37	0.43
0.167	0.0	0.11	0.08	0.05	0.05	0.05	0.05	0.06	0.07	0.19	0.28	0.37	0.42
0.25	0.0	0.10	0.07	0.05	0.05	0.05	0.05	0.06	0.07	0.17	0.27	0.35	0.41
0.50	0.0	0.08	0.07	0.06	0.07	0.06	0.05	0.06	0.07	0.13	0.19	0.23	0.24
1.0	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.0	0.0	0.57	0.55	0.61	0.87	1.00	1.20	1.30	1.30	1.30	1.28	1.24	1.20
4.0	0.0	2.60	2.84	3.92	5.72	7.20	8.32	9.28	9.92	10.24	10.24	10.24	10.24
6.0	0.0	6.57	6.75	10.62	15.84	18.90	22.50	25.74	27.90	28.44	28.44	28.35	28.26
10.0	0.0	17.25	18.75	30.00	45.00	53.00	63.50	75.00	84.00	89.00	89.00	88.50	88.00
16.0	0.0	42.75	48.13	77.57	116.74	136.45	164.10	196.86	224.26	241.92	241.92	240.38	238.59

**SD5-1 Wye, 45 Degree, Diverging**

		<i>C<sub>b</sub></i> Values								
		<i>Q<sub>b</sub>/Q<sub>c</sub></i>								
<i>A<sub>b</sub>/A<sub>c</sub></i>		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1		0.38	0.38	0.48	0.45	0.40	0.36	0.32	0.29	0.26
0.2		2.25	0.38	0.31	0.38	0.47	0.48	0.47	0.45	0.42
0.3		6.29	1.02	0.38	0.30	0.33	0.38	0.45	0.48	0.48
0.4		12.41	2.25	0.74	0.38	0.30	0.31	0.35	0.38	0.44
0.5		20.58	4.01	1.37	0.62	0.38	0.30	0.30	0.32	0.36
0.6		30.78	6.29	2.25	1.02	0.56	0.38	0.31	0.30	0.31
0.7		43.02	9.10	3.36	1.57	0.85	0.52	0.38	0.31	0.30
0.8		57.29	12.41	4.71	2.25	1.22	0.74	0.50	0.38	0.32
0.9		73.59	16.24	6.29	3.06	1.69	1.02	0.67	0.48	0.38
1.0		91.92	20.58	8.11	4.01	2.25	1.37	0.90	0.62	0.47

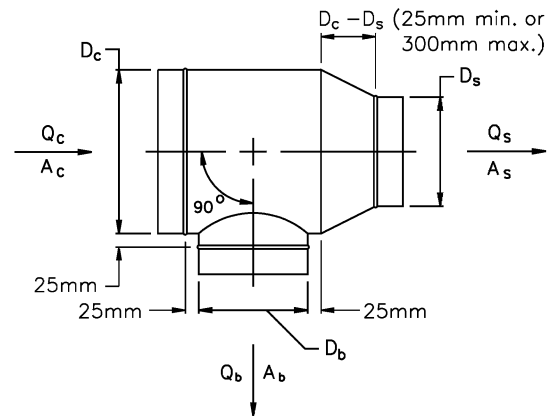
		<i>C<sub>s</sub></i> Values								
		<i>Q<sub>s</sub>/Q<sub>c</sub></i>								
<i>A<sub>s</sub>/A<sub>c</sub></i>		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1		0.13	0.24	0.57	0.74	0.74	0.70	0.65	0.60	0.56
0.2		0.20	0.13	0.15	0.16	0.28	0.57	0.69	0.74	0.75
0.3		0.90	0.14	0.13	0.14	0.15	0.16	0.20	0.42	0.57
0.4		2.88	0.20	0.14	0.13	0.14	0.15	0.15	0.16	0.34
0.5		6.25	0.38	0.17	0.14	0.13	0.14	0.14	0.15	0.15
0.6		11.88	0.90	0.20	0.14	0.14	0.13	0.14	0.14	0.15
0.7		18.62	1.72	0.33	0.18	0.16	0.14	0.13	0.15	0.14
0.8		26.88	2.88	0.50	0.20	0.15	0.14	0.13	0.13	0.14
0.9		36.45	4.46	0.90	0.30	0.19	0.16	0.15	0.14	0.13
1.0		45.00	6.25	1.44	0.38	0.20	0.17	0.12	0.13	0.14



**SD5-9 Tee, Diverging**

		<i>C<sub>b</sub></i> Values								
		<i>Q<sub>b</sub>/Q<sub>c</sub></i>								
<i>A<sub>b</sub>/A<sub>c</sub></i>		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1		1.20	0.62	0.80	1.28	1.99	2.92	4.07	5.44	7.02
0.2		4.10	1.20	0.72	0.62	0.66	0.80	1.01	1.28	1.60
0.3		8.99	2.40	1.20	0.81	0.66	0.62	0.64	0.70	0.80
0.4		15.89	4.10	1.94	1.20	0.88	0.72	0.64	0.62	0.63
0.5		24.80	6.29	2.91	1.74	1.20	0.92	0.77	0.68	0.63
0.6		35.73	8.99	4.10	2.40	1.62	1.20	0.96	0.81	0.72
0.7		48.67	12.19	5.51	3.19	2.12	1.55	1.20	0.99	0.85
0.8		63.63	15.89	7.14	4.10	2.70	1.94	1.49	1.20	1.01
0.9		80.60	20.10	8.99	5.13	3.36	2.40	1.83	1.46	1.20
1.0		99.60	24.80	11.07	6.29	4.10	2.91	2.20	1.74	1.43

		<i>C<sub>s</sub></i> Values								
		<i>Q<sub>s</sub>/Q<sub>c</sub></i>								
<i>A<sub>s</sub>/A<sub>c</sub></i>		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1		0.13	0.24	0.57	0.74	0.74	0.70	0.65	0.60	0.56
0.2		0.20	0.13	0.15	0.16	0.28	0.57	0.69	0.74	0.75
0.3		0.90	0.14	0.13	0.14	0.15	0.16	0.20	0.42	0.57
0.4		2.88	0.20	0.14	0.13	0.14	0.15	0.15	0.16	0.34
0.5		6.25	0.38	0.17	0.14	0.13	0.14	0.14	0.15	0.15
0.6		11.88	0.90	0.20	0.14	0.14	0.13	0.14	0.14	0.15
0.7		18.62	1.72	0.33	0.18	0.16	0.14	0.13	0.15	0.14
0.8		26.88	2.88	0.50	0.20	0.15	0.14	0.13	0.13	0.14
0.9		36.45	4.46	0.90	0.30	0.19	0.16	0.15	0.14	0.13
1.0		45.00	6.25	1.44	0.38	0.20	0.17	0.12	0.13	0.14

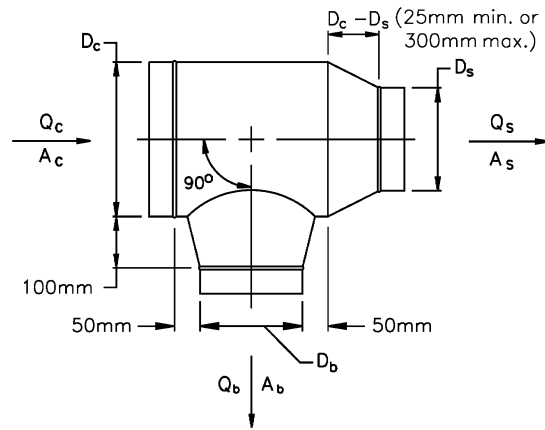




**SD5-10 Tee, Conical Branch Tapered into Body, Diverging**

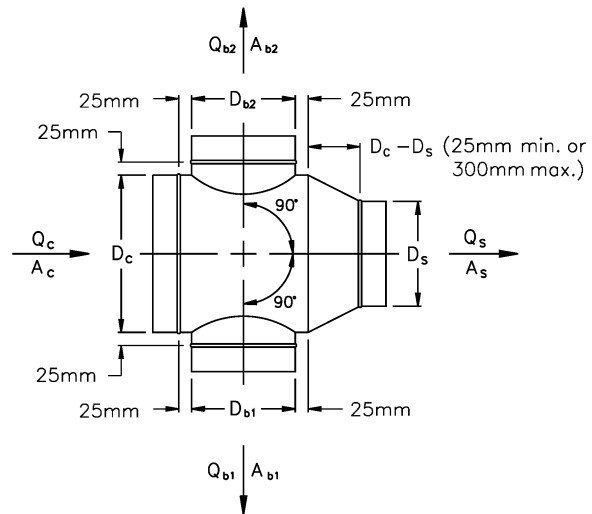
<i>C<sub>b</sub></i> Values									
<i>A<sub>b</sub>/A<sub>c</sub></i>	<i>Q<sub>b</sub>/Q<sub>c</sub></i>								
	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1	0.65	0.24	0.15	0.11	0.09	0.07	0.06	0.05	0.05
0.2	2.98	0.65	0.33	0.24	0.18	0.15	0.13	0.11	0.10
0.3	7.36	1.56	0.65	0.39	0.29	0.24	0.20	0.17	0.15
0.4	13.78	2.98	1.20	0.65	0.43	0.33	0.27	0.24	0.21
0.5	22.24	4.92	1.98	1.04	0.65	0.47	0.36	0.31	0.27
0.6	32.73	7.36	2.98	1.56	0.96	0.65	0.49	0.39	0.33
0.7	45.26	10.32	4.21	2.21	1.34	0.90	0.65	0.51	0.42
0.8	59.82	13.78	5.67	2.98	1.80	1.20	0.86	0.65	0.52
0.9	76.41	17.75	7.36	3.88	2.35	1.56	1.11	0.83	0.65
1.0	95.04	22.24	9.27	4.92	2.98	1.98	1.40	1.04	0.81

<i>C<sub>s</sub></i> Values									
<i>A<sub>s</sub>/A<sub>c</sub></i>	<i>Q<sub>s</sub>/Q<sub>c</sub></i>								
	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1	0.13	0.24	0.57	0.74	0.74	0.70	0.65	0.60	0.56
0.2	0.20	0.13	0.15	0.16	0.28	0.57	0.69	0.74	0.75
0.3	0.90	0.14	0.13	0.14	0.15	0.16	0.20	0.42	0.57
0.4	2.88	0.20	0.14	0.13	0.14	0.15	0.15	0.16	0.34
0.5	6.25	0.38	0.17	0.14	0.13	0.14	0.14	0.15	0.15
0.6	11.88	0.90	0.20	0.14	0.14	0.13	0.14	0.14	0.15
0.7	18.62	1.72	0.33	0.18	0.16	0.14	0.13	0.15	0.14
0.8	26.88	2.88	0.50	0.20	0.15	0.14	0.13	0.13	0.14
0.9	36.45	4.46	0.90	0.30	0.19	0.16	0.15	0.14	0.13
1.0	45.00	6.25	1.44	0.38	0.20	0.17	0.12	0.13	0.14



**SD5-24 Cross, Diverging**

<i>C<sub>b1</sub></i> Values										
<i>A<sub>s</sub>/A<sub>c</sub></i>	<i>A<sub>b1</sub>/A<sub>c</sub></i>	<i>Q<sub>b1</sub>/Q<sub>c</sub></i>								
		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.20	0.1	2.07	2.08	1.62	1.30	1.99	2.92	4.07	5.44	7.02
	0.2	4.10	2.07	2.31	2.08	1.83	1.62	1.44	1.30	1.60
	0.3	8.99	2.40	2.07	2.34	2.24	2.08	1.91	1.76	1.62
	0.4	15.89	4.10	1.94	2.07	2.32	2.31	2.21	2.08	1.95
	0.5	24.80	6.29	2.91	1.74	2.07	2.30	2.33	2.27	2.18
	0.6	35.73	8.99	4.10	2.40	1.62	2.07	2.29	2.34	2.31
	0.7	48.67	12.19	5.51	3.19	2.12	1.60	2.07	2.27	2.33
	0.8	63.63	15.89	7.14	4.10	2.70	1.94	1.68	2.07	2.25
	0.9	80.60	20.10	8.99	5.13	3.36	2.40	1.83	1.74	2.07
	1.0	99.60	24.80	11.07	6.29	4.10	2.91	2.20	1.74	1.78
0.35	0.1	1.20	3.25	3.11	2.69	2.32	2.92	4.07	5.44	7.02
	0.2	4.10	1.20	2.44	3.25	3.28	3.11	2.90	2.69	2.49
	0.3	8.99	2.40	1.20	1.69	2.88	3.25	3.31	3.23	3.11
	0.4	15.89	4.10	1.94	1.20	1.12	2.44	3.02	3.25	3.31
	0.5	24.80	6.29	2.91	1.74	1.20	0.92	2.04	2.73	3.09
	0.6	35.73	8.99	4.10	2.40	1.62	1.20	0.96	1.69	2.44
	0.7	48.67	12.19	5.51	3.19	2.12	1.55	1.20	0.99	1.38
	0.8	63.63	15.89	7.14	4.10	2.70	1.94	1.49	1.20	1.01
	0.9	80.60	20.10	8.99	5.13	3.36	2.40	1.83	1.46	1.20
	1.0	99.60	24.80	11.07	6.29	4.10	2.91	2.20	1.74	1.43
0.55	0.1	1.20	0.62	0.80	1.28	1.99	2.92	4.07	5.44	7.02
	0.2	4.10	1.20	0.72	0.62	0.66	0.80	1.01	1.28	1.60
	0.3	8.99	2.40	1.20	0.81	0.66	0.62	0.64	0.70	0.80
	0.4	15.89	4.10	1.94	1.20	0.88	0.72	0.64	0.62	0.63
	0.5	24.80	6.29	2.91	1.74	1.20	0.92	0.77	0.68	0.63
	0.6	35.73	8.99	4.10	2.40	1.62	1.20	0.96	0.81	0.72
	0.7	48.67	12.19	5.51	3.19	2.12	1.55	1.20	0.99	0.85
	0.8	63.63	15.89	7.14	4.10	2.70	1.94	1.49	1.20	1.01
	0.9	80.60	20.10	8.99	5.13	3.36	2.40	1.83	1.46	1.20
	1.0	99.60	24.80	11.07	6.29	4.10	2.91	2.20	1.74	1.43



SD5-24 Cross, Diverging (Continued)

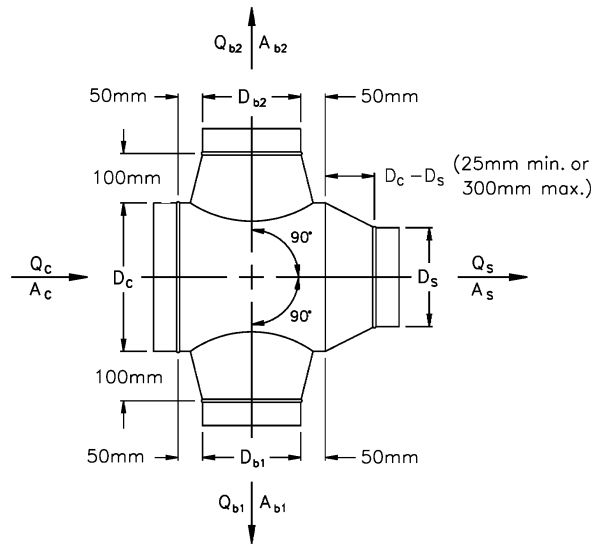
		$C_{b1}$ Values (Concluded)								
		$Q_{b1}/Q_c$								
$A_s/A_c$	$A_{b1}/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.80	0.1	1.20	0.62	0.80	1.28	1.99	2.92	4.07	5.44	7.02
	0.2	4.10	1.20	0.72	0.62	0.66	0.80	1.01	1.28	1.60
	0.3	8.99	2.40	1.20	0.81	0.66	0.62	0.64	0.70	0.80
	0.4	15.89	4.10	1.94	1.20	0.88	0.72	0.64	0.62	0.63
	0.5	24.80	6.29	2.91	1.74	1.20	0.92	0.77	0.68	0.63
	0.6	35.73	8.99	4.10	2.40	1.62	1.20	0.96	0.81	0.72
	0.7	48.67	12.19	5.51	3.19	2.12	1.55	1.20	0.99	0.85
	0.8	63.63	15.89	7.14	4.10	2.70	1.94	1.49	1.20	1.01
	0.9	80.60	20.10	8.99	5.13	3.36	2.40	1.83	1.46	1.20
	1.0	99.60	24.80	11.07	6.29	4.10	2.91	2.20	1.74	1.43
1.00	0.1	1.20	0.62	0.80	1.28	1.99	2.92	4.07	5.44	7.02
	0.2	4.10	1.20	0.72	0.62	0.66	0.80	1.01	1.28	1.60
	0.3	8.99	2.40	1.20	0.81	0.66	0.62	0.64	0.70	0.80
	0.4	15.89	4.10	1.94	1.20	0.88	0.72	0.64	0.62	0.63
	0.5	24.80	6.29	2.91	1.74	1.20	0.92	0.77	0.68	0.63
	0.6	35.73	8.99	4.10	2.40	1.62	1.20	0.96	0.81	0.72
	0.7	48.67	12.19	5.51	3.19	2.12	1.55	1.20	0.99	0.85
	0.8	63.63	15.89	7.14	4.10	2.70	1.94	1.49	1.20	1.01
	0.9	80.60	20.10	8.99	5.13	3.36	2.40	1.83	1.46	1.20
	1.0	99.60	24.80	11.07	6.29	4.10	2.91	2.20	1.74	1.43

		$C_s$ Values								
		$Q_s/Q_c$								
$A_s/A_c$		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1		0.13	0.24	0.57	0.74	0.74	0.70	0.65	0.60	0.56
0.2		0.20	0.13	0.15	0.16	0.28	0.57	0.69	0.74	0.75
0.3		0.90	0.14	0.13	0.14	0.15	0.16	0.20	0.42	0.57
0.4		2.88	0.20	0.14	0.13	0.14	0.15	0.15	0.16	0.34
0.5		6.25	0.38	0.17	0.14	0.13	0.14	0.14	0.15	0.15
0.6		11.88	0.90	0.20	0.14	0.14	0.13	0.14	0.14	0.15
0.7		18.62	1.72	0.33	0.18	0.16	0.14	0.13	0.15	0.14
0.8		26.88	2.88	0.50	0.20	0.15	0.14	0.13	0.13	0.14
0.9		36.45	4.46	0.90	0.30	0.19	0.16	0.15	0.14	0.13
1.0		45.00	6.25	1.44	0.38	0.20	0.17	0.12	0.13	0.14

For the other branch, subscripts 1 and 2 change places.

SD5-25 Cross, Conical Branches Tapered into Body, Diverging

		$C_{b1}$ Values								
		$Q_{b1}/Q_c$								
$A_s/A_c$	$A_{b1}/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.20	0.1	2.07	2.08	1.62	1.30	1.08	0.93	0.81	0.72	0.64
	0.2	2.98	2.07	2.31	2.08	1.83	1.62	1.44	1.30	1.18
	0.3	7.36	1.56	2.07	2.34	2.24	2.08	1.91	1.76	1.62
	0.4	13.78	2.98	1.20	2.07	2.32	2.31	2.21	2.08	1.95
	0.5	22.24	4.92	1.98	1.28	2.07	2.30	2.33	2.27	2.18
	0.6	32.73	7.36	2.98	1.56	1.48	2.07	2.29	2.34	2.31
	0.7	45.26	10.32	4.21	2.21	1.34	1.60	2.07	2.27	2.33
	0.8	59.82	13.78	5.67	2.98	1.80	1.20	1.68	2.07	2.25
	0.9	76.41	17.75	7.36	3.88	2.35	1.56	1.12	1.74	2.07
	1.0	95.04	22.24	9.27	4.92	2.98	1.98	1.40	1.28	1.78
0.35	0.1	0.65	3.25	3.11	2.69	2.32	2.03	1.80	1.61	1.46
	0.2	2.98	0.65	2.44	3.25	3.28	3.11	2.90	2.69	2.49
	0.3	7.36	1.56	0.65	1.69	2.88	3.25	3.31	3.23	3.11
	0.4	13.78	2.98	1.20	0.65	1.12	2.44	3.02	3.25	3.31
	0.5	22.24	4.92	1.98	1.04	0.65	0.69	2.04	2.73	3.09
	0.6	32.73	7.36	2.98	1.56	0.96	0.65	0.49	1.69	2.44
	0.7	45.26	10.32	4.21	2.21	1.34	0.90	0.65	0.51	1.38
	0.8	59.82	13.78	5.67	2.98	1.80	1.20	0.86	0.65	0.52
	0.9	76.41	17.75	7.36	3.88	2.35	1.56	1.11	0.83	0.65
	1.0	95.04	22.24	9.27	4.92	2.98	1.98	1.40	1.04	0.81
0.55	0.1	0.65	1.50	1.56	1.38	1.20	1.06	0.94	0.84	0.77
	0.2	2.98	0.65	0.89	1.50	1.60	1.56	1.47	1.38	1.28
	0.3	7.36	1.56	0.65	0.39	1.20	1.50	1.59	1.59	1.56
	0.4	13.78	2.98	1.20	0.65	0.43	0.89	1.31	1.50	1.58
	0.5	22.24	4.92	1.98	1.04	0.65	0.47	0.61	1.09	1.36
	0.6	32.73	7.36	2.98	1.56	0.96	0.65	0.49	0.39	0.89
	0.7	45.26	10.32	4.21	2.21	1.34	0.90	0.65	0.51	0.42
	0.8	59.82	13.78	5.67	2.98	1.80	1.20	0.86	0.65	0.52
	0.9	76.41	17.75	7.36	3.88	2.35	1.56	1.11	0.83	0.65
	1.0	95.04	22.24	9.27	4.92	2.98	1.98	1.40	1.04	0.81



SD5-25 Cross, Conical Branches Tapered into Body, Diverging (Continued)

		$C_{b1}$ Values (Concluded)									
		$Q_{b1}/Q_c$									
$A_s/A_c$	$A_{b1}/A_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	
0.80	0.1	0.65	0.24	0.15	0.11	0.09	0.07	0.06	0.05	0.05	
	0.2	2.98	0.65	0.33	0.24	0.18	0.15	0.13	0.11	0.10	
	0.3	7.36	1.56	0.65	0.39	0.29	0.24	0.20	0.17	0.15	
	0.4	13.78	2.98	1.20	0.65	0.43	0.33	0.27	0.24	0.21	
	0.5	22.24	4.92	1.98	1.04	0.65	0.47	0.36	0.31	0.27	
	0.6	32.73	7.36	2.98	1.56	0.96	0.65	0.49	0.39	0.33	
	0.7	45.26	10.32	4.21	2.21	1.34	0.90	0.65	0.51	0.42	
	0.8	59.82	13.78	5.67	2.98	1.80	1.20	0.86	0.65	0.52	
	0.9	76.41	17.75	7.36	3.88	2.35	1.56	1.11	0.83	0.65	
	1.0	95.04	22.24	9.27	4.92	2.98	1.98	1.40	1.04	0.81	
1.00	0.1	0.65	0.24	0.15	0.11	0.09	0.07	0.06	0.05	0.05	
	0.2	2.98	0.65	0.33	0.24	0.18	0.15	0.13	0.11	0.10	
	0.3	7.36	1.56	0.65	0.39	0.29	0.24	0.20	0.17	0.15	
	0.4	13.78	2.98	1.20	0.65	0.43	0.33	0.27	0.24	0.21	
	0.5	22.24	4.92	1.98	1.04	0.65	0.47	0.36	0.31	0.27	
	0.6	32.73	7.36	2.98	1.56	0.96	0.65	0.49	0.39	0.33	
	0.7	45.26	10.32	4.21	2.21	1.34	0.90	0.65	0.51	0.42	
	0.8	59.82	13.78	5.67	2.98	1.80	1.20	0.86	0.65	0.52	
	0.9	76.41	17.75	7.36	3.88	2.35	1.56	1.11	0.83	0.65	
	1.0	95.04	22.24	9.27	4.92	2.98	1.98	1.40	1.04	0.81	

		$C_s$ Values									
		$Q_s/Q_c$									
$A_s/A_c$		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	
0.1		0.13	0.24	0.57	0.74	0.74	0.70	0.65	0.60	0.56	
0.2		0.20	0.13	0.15	0.16	0.28	0.57	0.69	0.74	0.75	
0.3		0.90	0.14	0.13	0.14	0.15	0.16	0.20	0.42	0.57	
0.4		2.88	0.20	0.14	0.13	0.14	0.15	0.15	0.16	0.34	
0.5		6.25	0.38	0.17	0.14	0.13	0.14	0.14	0.15	0.15	
0.6		11.88	0.90	0.20	0.14	0.14	0.13	0.14	0.14	0.15	
0.7		18.62	1.72	0.33	0.18	0.16	0.14	0.13	0.15	0.14	
0.8		26.88	2.88	0.50	0.20	0.15	0.14	0.13	0.13	0.14	
0.9		36.45	4.46	0.90	0.30	0.19	0.16	0.15	0.14	0.13	
1.0		45.00	6.25	1.44	0.38	0.20	0.17	0.12	0.13	0.14	

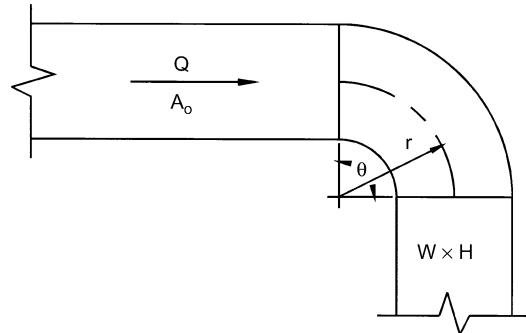
For the other branch, subscripts 1 and 2 change places

RECTANGULAR FITTINGS

CR3-1 Elbow, Smooth Radius, Without Vanes

		$C_p$ Values										
		$H/W$										
$r/W$		0.25	0.50	0.75	1.0	1.50	2.0	3.0	4.0	5.0	6.0	8.0
0.50		1.53	1.38	1.29	1.18	1.06	1.00	1.00	1.06	1.12	1.16	1.18
0.75		0.57	0.52	0.48	0.44	0.40	0.39	0.39	0.40	0.42	0.43	0.44
1.00		0.27	0.25	0.23	0.21	0.19	0.18	0.18	0.19	0.20	0.21	0.21
1.50		0.22	0.20	0.19	0.17	0.15	0.14	0.14	0.15	0.16	0.17	0.17
2.00		0.20	0.18	0.16	0.15	0.14	0.13	0.13	0.14	0.14	0.15	0.15
		Angle Factor $K$										
$\theta$		0	20	30	45	60	75	90	110	130	150	180
$K$		0.00	0.31	0.45	0.60	0.78	0.90	1.00	1.13	1.20	1.28	1.40

$C_o = KC_p$  where  $K$  = angle factor



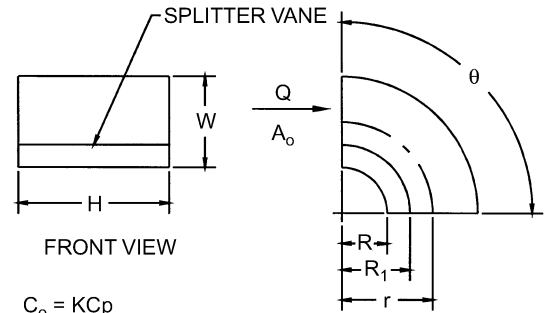
**CR3-3 Elbow, Smooth Radius, One Splitter Vane**

$r/W$	$C_p$ Values										
	0.25	0.50	1.0	1.50	2.0	3.0	4.0	5.0	6.0	7.0	8.0
0.55	0.52	0.40	0.43	0.49	0.55	0.66	0.75	0.84	0.93	1.01	1.09
0.60	0.36	0.27	0.25	0.28	0.30	0.35	0.39	0.42	0.46	0.49	0.52
0.65	0.28	0.21	0.18	0.19	0.20	0.22	0.25	0.26	0.28	0.30	0.32
0.70	0.22	0.16	0.14	0.14	0.15	0.16	0.17	0.18	0.19	0.20	0.21
0.75	0.18	0.13	0.11	0.11	0.11	0.12	0.13	0.14	0.14	0.15	0.15
0.80	0.15	0.11	0.09	0.09	0.09	0.09	0.10	0.10	0.11	0.11	0.12
0.85	0.13	0.09	0.08	0.07	0.07	0.08	0.08	0.08	0.08	0.09	0.09
0.90	0.11	0.08	0.07	0.06	0.06	0.06	0.06	0.07	0.07	0.07	0.07
0.95	0.10	0.07	0.06	0.05	0.05	0.05	0.05	0.05	0.06	0.06	0.06
1.00	0.09	0.06	0.05	0.05	0.04	0.04	0.04	0.05	0.05	0.05	0.05

Angle Factor $K$					
$\theta$	0	30	45	60	90
$K$	0.00	0.45	0.60	0.78	1.00

Curve Ratio CR										
$r/W$	0.55	0.60	0.65	0.70	0.75	0.80	0.85	0.90	0.95	1.0
CR	0.218	0.302	0.361	0.408	0.447	0.480	0.509	0.535	0.557	0.577

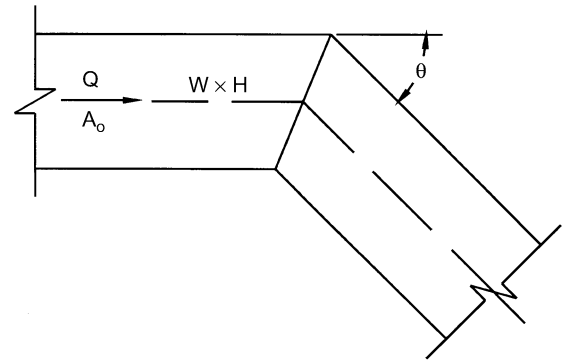
Throat Radius/Width Ratio ( $R/W$ )										
$r/W$	0.55	0.60	0.65	0.70	0.75	0.80	0.85	0.90	0.95	1.0
$R/W$	0.05	0.10	0.15	0.20	0.25	0.30	0.35	0.40	0.45	0.50



$C_o = KC_p$   
 $R_1 = R/CR$   
 where  
 $R$  = throat radius  
 $R_1$  = splitter vane radius  
 $CR$  = curve ratio  
 $K$  = angle factor

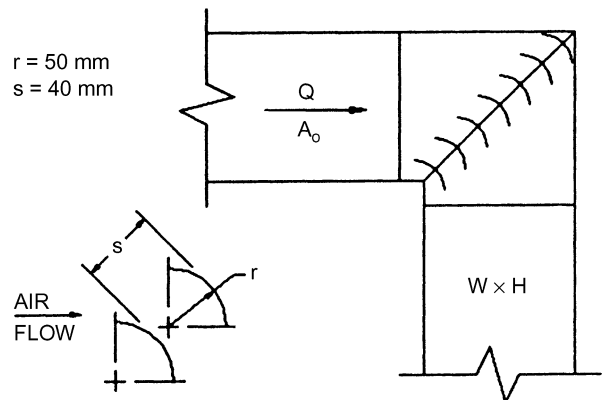
**CR3-6 Elbow, Mitered**

$\theta$	$C_o$ Values										
	0.25	0.50	0.75	1.00	1.50	2.0	3.0	4.0	5.0	6.0	8.0
20	0.08	0.08	0.08	0.07	0.07	0.07	0.06	0.06	0.05	0.05	0.05
30	0.18	0.17	0.17	0.16	0.15	0.15	0.13	0.13	0.12	0.12	0.11
45	0.38	0.37	0.36	0.34	0.33	0.31	0.28	0.27	0.26	0.25	0.24
60	0.60	0.59	0.57	0.55	0.52	0.49	0.46	0.43	0.41	0.39	0.38
75	0.89	0.87	0.84	0.81	0.77	0.73	0.67	0.63	0.61	0.58	0.57
90	1.30	1.27	1.23	1.18	1.13	1.07	0.98	0.92	0.89	0.85	0.83



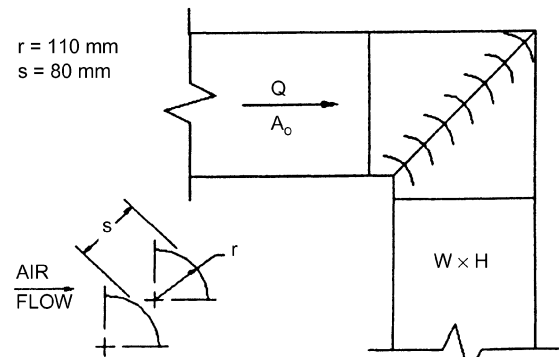
**CR3-9 Elbow, Mitered, 90 Degree, Single-Thickness Vanes (40 mm Vane Spacing)**

$C_o = 0.11$



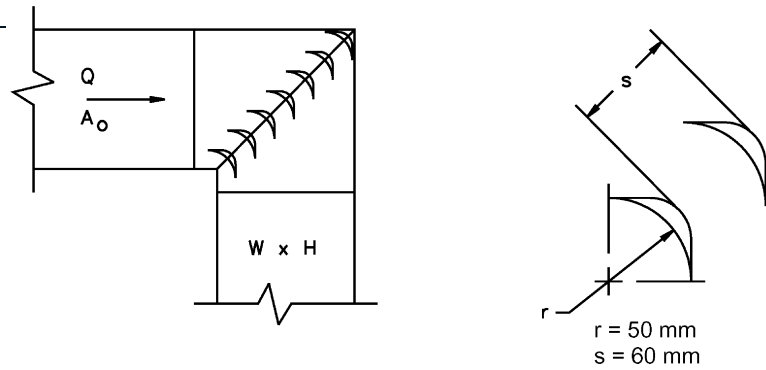
**CR3-12 Elbow, Mitered, 90 Degree, Single-Thickness Vanes  
(80 mm Vane Spacing)**

$C_o = 0.33$



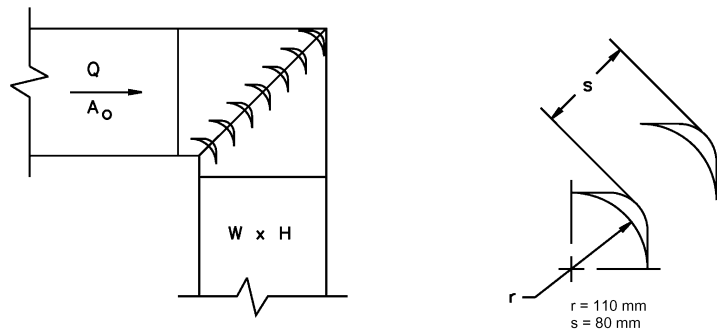
**CR3-15 Elbow, Mitered, 90 Degree, Double-Thickness Vanes (60 mm Vane Spacing)**

$C_o = 0.25$



**CR3-16 Elbow, Mitered, 90 Degree, Double-Thickness Vanes (80 mm Vane Spacing)**

$C_o = 0.41$

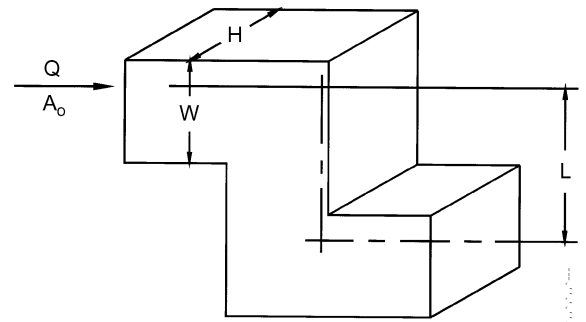


**CR3-17 Elbow, Z-Shaped**

		$C_p$ Values												
		$L/W$												
$H/W$		0.0	0.4	0.6	0.8	1.0	1.2	1.4	1.6	1.8	2.0	4.0	8.0	10.0
0.25	0.0	0.68	0.99	1.77	2.89	3.97	4.41	4.60	4.64	4.60	3.39	3.03	2.70	
0.50	0.0	0.66	0.96	1.72	2.81	3.86	4.29	4.47	4.52	4.47	3.30	2.94	2.62	
0.75	0.0	0.64	0.94	1.67	2.74	3.75	4.17	4.35	4.39	4.35	3.20	2.86	2.55	
1.0	0.0	0.62	0.90	1.61	2.63	3.61	4.01	4.18	4.22	4.18	3.08	2.75	2.45	
1.5	0.0	0.59	0.86	1.53	2.50	3.43	3.81	3.97	4.01	3.97	2.93	2.61	2.33	
2.0	0.0	0.56	0.81	1.45	2.37	3.25	3.61	3.76	3.80	3.76	2.77	2.48	2.21	
3.0	0.0	0.51	0.75	1.34	2.18	3.00	3.33	3.47	3.50	3.47	2.56	2.28	2.03	
4.0	0.0	0.48	0.70	1.26	2.05	2.82	3.13	3.26	3.29	3.26	2.40	2.15	1.91	
6.0	0.0	0.45	0.65	1.16	1.89	2.60	2.89	3.01	3.04	3.01	2.22	1.98	1.76	
8.0	0.0	0.43	0.63	1.13	1.84	2.53	2.81	2.93	2.95	2.93	2.16	1.93	1.72	

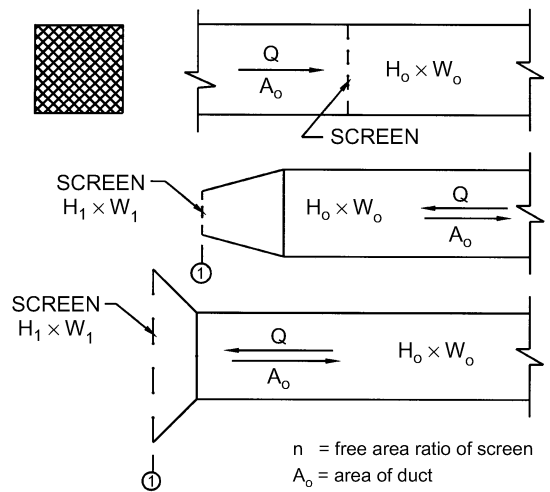
Reynolds Number Correction Factor $K_r$									
Re/1000	10	20	30	40	60	80	100	140	500
$K_r$	1.40	1.26	1.19	1.14	1.09	1.06	1.04	1.00	1.00



$C_o = K_r C_p$   
 where  $K_r$  = Reynolds number correction factor

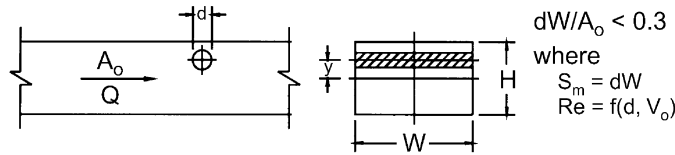
**CR6-1 Screen (Only)**

		$C_o$ Values													
		$n$													
$A_1/A_o$		0.30	0.35	0.40	0.45	0.50	0.55	0.60	0.65	0.70	0.75	0.80	0.90	1.0	
0.2	155.0	103.0	75.00	55.00	41.25	31.50	24.25	18.75	14.50	11.00	8.00	3.50	0.0		
0.3	68.89	45.56	33.33	24.44	18.33	14.00	10.78	8.33	6.44	4.89	3.56	1.56	0.0		
0.4	38.75	25.63	18.75	13.75	10.31	7.88	6.06	4.69	3.63	2.75	2.00	0.88	0.0		
0.5	24.80	16.40	12.00	8.80	6.60	5.04	3.88	3.00	2.32	1.76	1.28	0.56	0.0		
0.6	17.22	11.39	8.33	6.11	4.58	3.50	2.69	2.08	1.61	1.22	0.89	0.39	0.0		
0.7	12.65	8.37	6.12	4.49	3.37	2.57	1.98	1.53	1.18	0.90	0.65	0.29	0.0		
0.8	9.69	6.40	4.69	3.44	2.58	1.97	1.52	1.17	0.91	0.69	0.50	0.22	0.0		
0.9	7.65	5.06	3.70	2.72	2.04	1.56	1.20	0.93	0.72	0.54	0.40	0.17	0.0		
1.0	6.20	4.10	3.00	2.20	1.65	1.26	0.97	0.75	0.58	0.44	0.32	0.14	0.0		
1.2	4.31	2.85	2.08	1.53	1.15	0.88	0.67	0.52	0.40	0.31	0.22	0.10	0.0		
1.4	3.16	2.09	1.53	1.12	0.84	0.64	0.49	0.38	0.30	0.22	0.16	0.07	0.0		
1.6	2.42	1.60	1.17	0.86	0.64	0.49	0.38	0.29	0.23	0.17	0.13	0.05	0.0		
1.8	1.91	1.27	0.93	0.68	0.51	0.39	0.30	0.23	0.18	0.14	0.10	0.04	0.0		
2.0	1.55	1.03	0.75	0.55	0.41	0.32	0.24	0.19	0.15	0.11	0.08	0.04	0.0		
2.5	0.99	0.66	0.48	0.35	0.26	0.20	0.16	0.12	0.09	0.07	0.05	0.02	0.0		
3.0	0.69	0.46	0.33	0.24	0.18	0.14	0.11	0.08	0.06	0.05	0.04	0.02	0.0		
4.0	0.39	0.26	0.19	0.14	0.10	0.08	0.06	0.05	0.04	0.03	0.02	0.01	0.0		
6.0	0.17	0.11	0.08	0.06	0.05	0.04	0.03	0.02	0.02	0.01	0.01	0.00	0.0		



$n$  = free area ratio of screen  
 $A_o$  = area of duct  
 $A_1$  = cross-sectional area of duct or fitting where screen is located

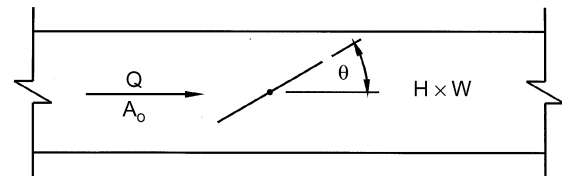
**CR6-4 Obstruction, Smooth Cylinder in Rectangular Duct**



y/H	Re/1000	C <sub>o</sub> Values					y/H	Re/1000	C <sub>o</sub> Values					
		0.0	0.05	0.10	0.15	0.20			0.0	0.05	0.10	0.15	0.20	
0.00	0.1	0.0	0.10	0.21	0.35	0.47	0.25	400	0.0	0.04	0.10	0.16	0.21	
	0.5	0.0	0.08	0.17	0.28	0.38		500	0.0	0.03	0.07	0.12	0.16	
	200	0.0	0.08	0.17	0.28	0.38		600	0.0	0.02	0.04	0.06	0.09	
	300	0.0	0.07	0.16	0.26	0.35		1000	0.0	0.02	0.04	0.07	0.09	
	400	0.0	0.05	0.11	0.19	0.25		0.30	0.1	0.0	0.08	0.17	0.28	0.38
	500	0.0	0.04	0.09	0.14	0.19			0.5	0.0	0.06	0.14	0.22	0.30
	600	0.0	0.02	0.05	0.07	0.10			200	0.0	0.06	0.14	0.22	0.30
0.05	0.1	0.0	0.10	0.21	0.34	0.46	0.35	300	0.0	0.06	0.12	0.20	0.28	
	0.5	0.0	0.08	0.17	0.27	0.37		400	0.0	0.04	0.09	0.15	0.20	
	200	0.0	0.08	0.17	0.27	0.37		500	0.0	0.03	0.07	0.11	0.15	
	300	0.0	0.07	0.15	0.25	0.34		600	0.0	0.02	0.04	0.06	0.08	
	400	0.0	0.05	0.11	0.18	0.24		1000	0.0	0.02	0.04	0.06	0.09	
	500	0.0	0.04	0.08	0.13	0.18		0.40	0.1	0.0	0.07	0.16	0.26	0.35
	600	0.0	0.02	0.04	0.07	0.10			0.5	0.0	0.06	0.13	0.21	0.28
1000	0.0	0.02	0.05	0.08	0.11	200	0.0		0.06	0.13	0.21	0.28		
0.10	0.1	0.0	0.09	0.20	0.32	0.44	0.40	300	0.0	0.05	0.12	0.19	0.26	
	0.5	0.0	0.07	0.16	0.26	0.35		400	0.0	0.04	0.08	0.14	0.19	
	200	0.0	0.07	0.16	0.26	0.35		500	0.0	0.03	0.06	0.10	0.14	
	300	0.0	0.07	0.15	0.24	0.32		600	0.0	0.02	0.03	0.05	0.07	
	400	0.0	0.05	0.11	0.17	0.23		1000	0.0	0.02	0.04	0.06	0.08	
	500	0.0	0.04	0.08	0.13	0.18		0.40	0.1	0.0	0.07	0.14	0.23	0.32
	600	0.0	0.02	0.04	0.07	0.09			0.5	0.0	0.05	0.11	0.19	0.25
1000	0.0	0.02	0.05	0.08	0.10	200	0.0		0.05	0.11	0.19	0.25		
0.15	0.1	0.0	0.09	0.19	0.31	0.42	0.40	300	0.0	0.05	0.11	0.17	0.23	
	0.5	0.0	0.07	0.15	0.25	0.34		400	0.0	0.04	0.08	0.12	0.17	
	200	0.0	0.07	0.15	0.25	0.34		500	0.0	0.03	0.06	0.09	0.13	
	300	0.0	0.06	0.14	0.23	0.31		600	0.0	0.01	0.03	0.05	0.07	
	400	0.0	0.05	0.10	0.17	0.22		1000	0.0	0.02	0.03	0.05	0.07	
	500	0.0	0.04	0.08	0.12	0.17		0.40	0.1	0.0	0.06	0.13	0.20	0.28
	600	0.0	0.02	0.04	0.07	0.09			0.5	0.0	0.05	0.10	0.16	0.22
1000	0.0	0.02	0.04	0.07	0.10	200	0.0		0.05	0.10	0.16	0.22		
0.20	0.1	0.0	0.08	0.18	0.29	0.40	0.40	300	0.0	0.04	0.09	0.15	0.20	
	0.5	0.0	0.07	0.14	0.24	0.32		400	0.0	0.03	0.07	0.11	0.15	
	200	0.0	0.07	0.14	0.24	0.32		500	0.0	0.02	0.05	0.08	0.11	
	300	0.0	0.06	0.13	0.22	0.29		600	0.0	0.01	0.03	0.04	0.06	

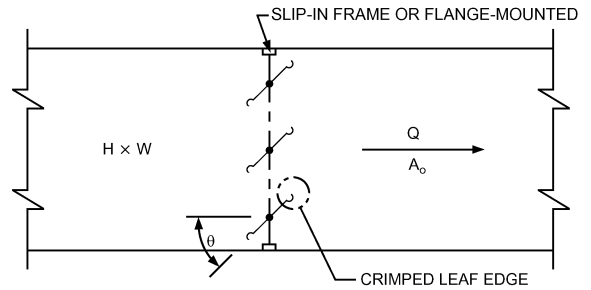
**CR9-1 Damper, Butterfly**

H/W	C <sub>o</sub> Values									
	θ									
	0	10	20	30	40	50	60	65	70	90
0.10	0.04	0.30	1.10	3.0	8.0	23.0	60.	100.	190.	9999
0.50	0.04	0.30	1.10	3.0	8.0	23.0	60.	100.	190.	9999
1.0	0.04	0.30	1.10	3.0	8.0	23.0	60.	100.	190.	9999
1.5	0.04	0.35	1.25	3.6	10.0	29.0	80.	155.	230.	9999
2.0	0.04	0.35	1.25	3.6	10.0	29.0	80.	155.	230.	9999



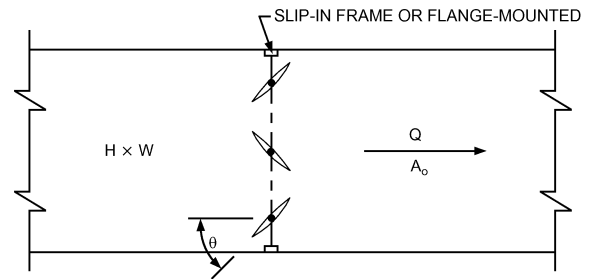
**CR9-3 Damper, Parallel and Opposed 3V Blades, Open**

$$C_o = 0.37$$



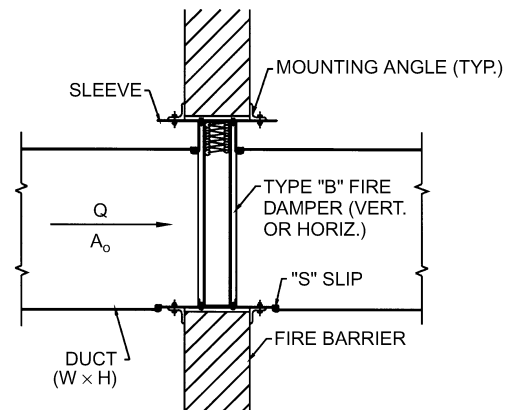
**CR9-4 Damper, Parallel and Opposed Airfoil Blades, Open**

$$C_o = 0.18$$



**CR9-6 Fire Damper, Curtain Type, Type B, Horizontal Duct**

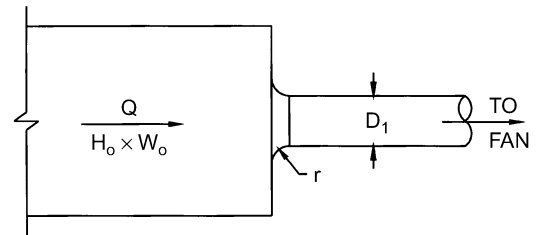
$$C_o = 0.19$$



**ER2-1 Bellmouth, Plenum to Round, Exhaust/Return Systems**

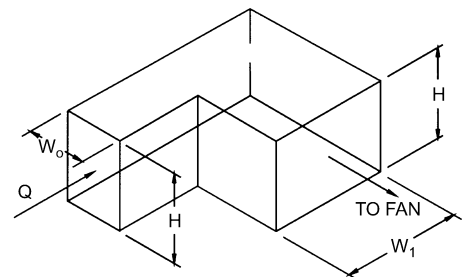
$r/D_1$	0.0	0.01	0.02	0.03	0.04	0.05	0.06	0.08	0.10	0.12	0.16	0.20	10.0
$C_l$	0.50	0.44	0.37	0.31	0.26	0.22	0.20	0.15	0.12	0.09	0.06	0.03	0.03

$$C_o = C_l \left( \frac{A_o}{A_1} \right)^2$$



**ER3-1 Elbow, 90 Degree, Variable Inlet/Outlet Areas, Exhaust/Return Systems**

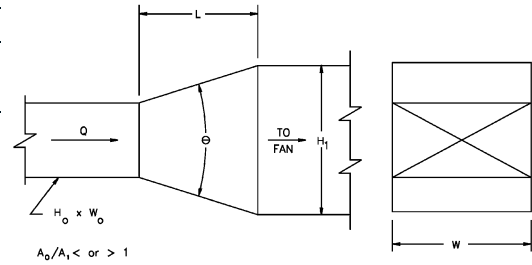
$H/W_o$	$C_o$ Values						
	$W_1/W_o$						
	0.6	0.8	1.0	1.2	1.4	1.6	2.0
0.25	1.76	1.43	1.24	1.14	1.09	1.06	1.06
1.00	1.70	1.36	1.15	1.02	0.95	0.90	0.84
4.00	1.46	1.10	0.90	0.81	0.76	0.72	0.66
100.00	1.50	1.04	0.79	0.69	0.63	0.60	0.55





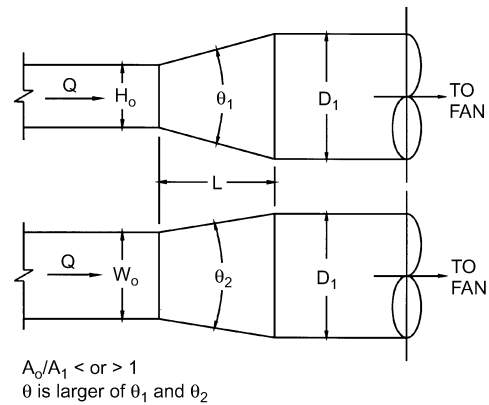
**ER4-1 Transition, Rectangular, Two Sides Parallel, Symmetrical, Exhaust/Return Systems**

		$C_o$ Values												
		$\theta$												
$A_o/A_1$		0	3	5	10	15	20	30	45	60	90	120	150	180
0.063	0.0	0.44	0.27	0.25	0.27	0.36	0.56	0.71	0.86	0.99	0.99	0.98	0.98	
0.10	0.0	0.41	0.27	0.23	0.25	0.34	0.53	0.69	0.83	0.94	0.94	0.92	0.91	
0.167	0.0	0.34	0.28	0.21	0.23	0.30	0.48	0.65	0.76	0.83	0.83	0.82	0.80	
0.25	0.0	0.26	0.29	0.17	0.19	0.25	0.42	0.60	0.68	0.70	0.70	0.68	0.66	
0.50	0.0	0.16	0.24	0.14	0.13	0.15	0.24	0.35	0.37	0.38	0.37	0.36	0.35	
1.00	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
2.00	0.0	0.30	0.38	0.25	0.17	0.17	0.17	0.23	0.29	0.49	0.66	0.81	0.88	
4.00	0.0	1.66	1.25	0.77	0.70	0.70	0.70	0.90	1.09	2.84	4.36	5.69	6.57	
6.00	0.0	4.05	3.14	1.76	1.58	1.58	1.58	2.12	2.66	6.71	10.11	13.13	15.20	
10.00	0.0	12.01	9.39	5.33	5.00	5.00	5.00	6.45	7.93	19.10	28.60	36.79	42.79	



**ER4-3 Transition, Rectangular to Round, Exhaust/Return Systems**

		$C_o$ Values												
		$\theta$												
$A_o/A_1$		0	3	5	10	15	20	30	45	60	90	120	150	180
0.063	0.0	0.17	0.19	0.30	0.46	0.53	0.64	0.77	0.88	0.95	0.95	0.94	0.93	
0.10	0.0	0.17	0.19	0.30	0.45	0.53	0.64	0.75	0.84	0.89	0.89	0.89	0.88	
0.167	0.0	0.18	0.19	0.30	0.44	0.53	0.63	0.72	0.78	0.79	0.79	0.79	0.79	
0.25	0.0	0.16	0.18	0.25	0.36	0.45	0.52	0.58	0.62	0.64	0.64	0.64	0.64	
0.50	0.0	0.14	0.14	0.15	0.22	0.25	0.30	0.33	0.33	0.33	0.32	0.31	0.30	
1.00	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
2.00	0.0	0.30	0.27	0.26	0.28	0.25	0.19	0.23	0.27	0.52	0.75	0.91	0.95	
4.00	0.0	1.60	1.14	0.84	0.85	0.86	0.76	0.90	1.09	2.78	4.30	5.65	6.55	
6.00	0.0	3.89	3.04	1.84	1.77	1.78	1.73	2.18	2.67	6.67	10.07	13.09	15.18	
10.00	0.0	11.80	9.31	5.40	5.18	5.15	5.05	6.44	7.94	19.06	28.55	36.75	42.75	

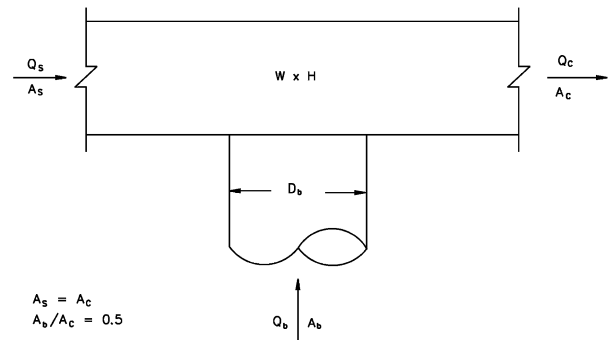


**ER5-2 Tee, Round Tap to Rectangular Main, Converging**

$Q_b/Q_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
$C_b$	-14.00	-2.38	0.50	0.65	1.03	1.17	1.19	1.33	1.51	1.44

$Q_s/Q_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
$C_s$	22.15	11.91	6.54	3.74	2.23	1.33	0.76	0.38	0.10	0.0

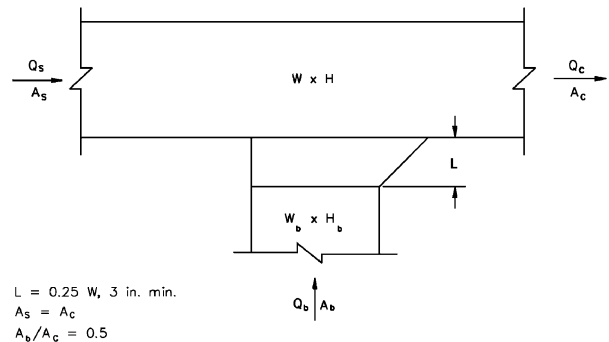


**ER5-3 Tee, 45 Degree Entry Branch, Converging**

$Q_b/Q_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
$C_b$	-19.38	-3.75	-0.74	0.48	0.66	0.75	0.85	0.77	0.83	0.83

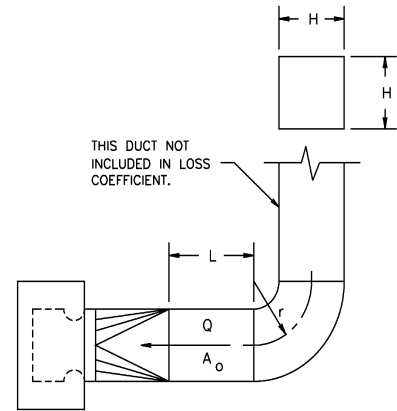
  

$Q_s/Q_c$	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0
$C_s$	22.15	11.91	6.54	3.74	2.23	1.33	0.76	0.38	0.10	0.0



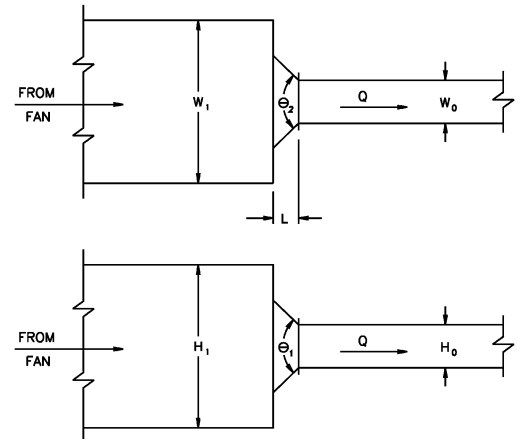
**ER7-1 Fan Inlet, Centrifugal, SWSI,  
90 Degree Smooth Radius Elbow (Square)**

<i>r/H</i>	<i>C<sub>o</sub></i> Values			
	<i>L/H</i>			
	0.0	2.0	5.0	10.0
0.50	2.50	1.60	0.80	0.80
0.75	2.00	1.20	0.67	0.67
1.00	1.20	0.67	0.33	0.33
1.50	1.00	0.57	0.30	0.30
2.00	0.80	0.47	0.26	0.26



**SR1-1 Conical Bellmouth/Sudden Contraction, Plenum to Rectangular,  
Supply Air Systems**

<i>L/D<sub>h</sub></i>	<i>C<sub>o</sub></i> Values								
	$\theta$								
	0	10	20	30	40	60	100	140	180
0.000	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
0.025	0.50	0.47	0.45	0.43	0.41	0.40	0.42	0.45	0.50
0.050	0.50	0.45	0.41	0.36	0.33	0.30	0.35	0.42	0.50
0.075	0.50	0.42	0.35	0.30	0.26	0.23	0.30	0.40	0.50
0.100	0.50	0.39	0.32	0.25	0.22	0.18	0.27	0.38	0.50
0.150	0.50	0.37	0.27	0.20	0.16	0.15	0.25	0.37	0.50
0.600	0.50	0.27	0.18	0.13	0.11	0.12	0.23	0.36	0.50

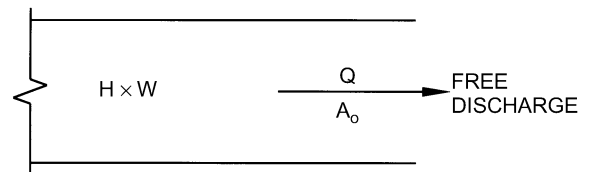


$$D_h = \frac{2 H_0 W_0}{(H_0 + W_0)}$$

$\theta$  IS LARGER OF  $\theta_1$  AND  $\theta_2$

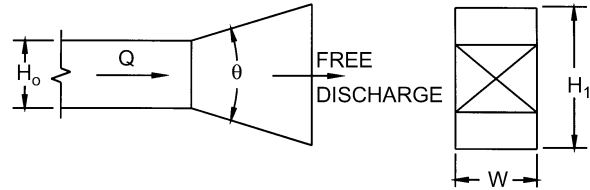
**SR2-1 Abrupt Exit**

Laminar Flow										
<i>H/W</i>	0.1	0.2	0.9	0.999	1.0	1.001	1.1	4.0	5.0	10.0
<i>C<sub>o</sub></i>	1.55	1.55	1.55	1.55	2.00	1.555	1.55	1.55	1.55	1.55
Turbulent Flow										
<i>C<sub>o</sub></i> = 1.0										



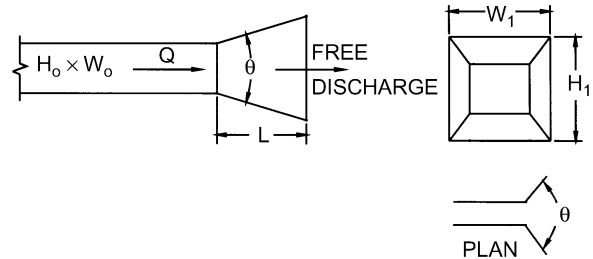
**SR2-3 Plain Diffuser (Two Sides Parallel), Free Discharge**

$A_1/A_o$	Re/1000	$C_o$ Values									
		$\theta$									
		4	8	10	14	20	30	45	60	90	120
1	50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	200	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	400	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	2000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	50	0.51	0.50	0.51	0.56	0.63	0.80	0.96	1.04	1.09	1.09
	100	0.48	0.48	0.50	0.56	0.63	0.80	0.96	1.04	1.09	1.09
	200	0.42	0.44	0.47	0.53	0.63	0.74	0.93	1.02	1.08	1.08
	400	0.38	0.40	0.42	0.50	0.62	0.74	0.93	1.02	1.08	1.08
	2000	0.38	0.40	0.42	0.50	0.62	0.74	0.93	1.02	1.08	1.08
4	50	0.35	0.34	0.38	0.48	0.63	0.76	0.91	1.03	1.07	1.07
	100	0.31	0.31	0.36	0.45	0.59	0.72	0.88	1.02	1.07	1.07
	200	0.27	0.26	0.31	0.41	0.53	0.67	0.83	0.96	1.06	1.06
	400	0.21	0.22	0.27	0.39	0.53	0.67	0.83	0.96	1.06	1.06
	2000	0.21	0.22	0.27	0.39	0.53	0.67	0.83	0.96	1.06	1.06
6	50	0.36	0.32	0.34	0.41	0.56	0.70	0.84	0.96	1.08	1.08
	100	0.32	0.27	0.30	0.41	0.56	0.70	0.84	0.96	1.08	1.08
	200	0.26	0.24	0.27	0.36	0.52	0.67	0.81	0.94	1.06	1.06
	400	0.21	0.20	0.24	0.36	0.52	0.67	0.81	0.94	1.06	1.06
	2000	0.21	0.18	0.24	0.34	0.50	0.67	0.81	0.94	1.05	1.05



**SR2-5 Pyramidal Diffuser, Free Discharge**

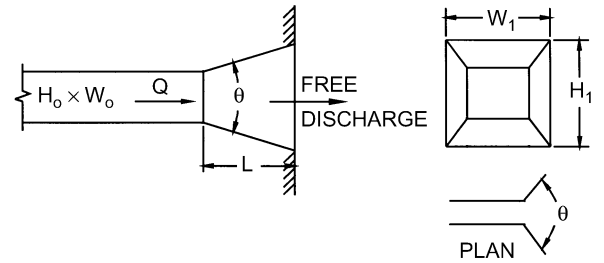
$A_1/A_o$	Re/1000	$C_o$ Values									
		$\theta$									
		4	8	10	14	20	30	45	60	90	120
1	50	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
	100	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
	200	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
	400	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
	2000	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
2	50	0.55	0.65	0.68	0.74	0.82	0.92	1.05	1.10	1.08	1.08
	100	0.51	0.61	0.66	0.73	0.81	0.90	1.04	1.09	1.08	1.08
	200	0.47	0.57	0.61	0.70	0.79	0.89	1.04	1.09	1.08	1.08
	400	0.42	0.50	0.56	0.64	0.76	0.88	1.02	1.07	1.08	1.08
	2000	0.42	0.50	0.56	0.64	0.76	0.88	1.02	1.07	1.08	1.08
4	50	0.38	0.53	0.60	0.69	0.78	0.90	1.02	1.07	1.09	1.09
	100	0.33	0.49	0.55	0.66	0.78	0.90	1.02	1.07	1.09	1.09
	200	0.27	0.42	0.50	0.62	0.74	0.87	1.00	1.06	1.08	1.08
	400	0.22	0.36	0.44	0.56	0.70	0.84	0.99	1.06	1.08	1.08
	2000	0.22	0.36	0.44	0.56	0.70	0.84	0.99	1.06	1.08	1.08
6	50	0.34	0.50	0.57	0.66	0.77	0.91	1.02	1.07	1.08	1.08
	100	0.30	0.47	0.54	0.63	0.76	0.98	1.02	1.07	1.08	1.08
	200	0.24	0.42	0.48	0.60	0.73	0.88	1.00	1.06	1.08	1.08
	400	0.18	0.34	0.44	0.56	0.73	0.86	0.98	1.06	1.08	1.08
	2000	0.18	0.34	0.44	0.56	0.73	0.86	0.98	1.06	1.08	1.08
10	50	0.30	0.45	0.53	0.64	0.74	0.85	0.97	1.10	1.12	1.12
	100	0.25	0.40	0.48	0.62	0.73	0.85	0.97	1.10	1.12	1.12
	200	0.20	0.34	0.44	0.56	0.69	0.82	0.95	1.10	1.11	1.11
	400	0.16	0.28	0.40	0.55	0.67	0.80	0.93	1.09	1.11	1.11
	2000	0.16	0.28	0.40	0.55	0.67	0.80	0.93	1.09	1.11	1.11



**SR2-6 Pyramidal Diffuser, with Wall**

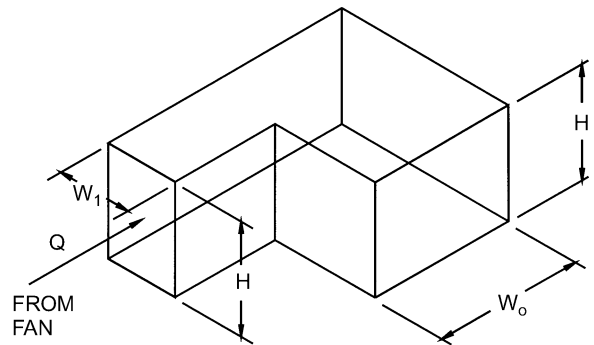
$L/D_h$	0.5	1.0	2.0	3.0	4.0	5.0	6.0	8.0	10.0	12.0	14.0
$C_o$	0.49	0.40	0.30	0.26	0.23	0.21	0.19	0.17	0.16	0.15	0.14
$\theta$	26	19	13	11	9	8	7	6	6	5	5

$\theta$  is the optimum angle.

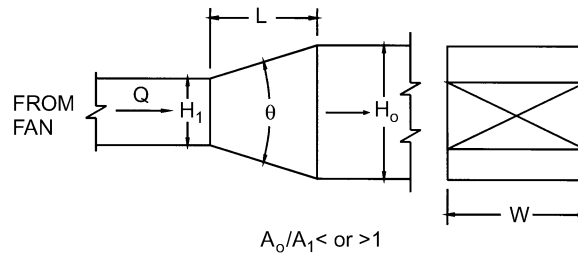


**SR3-1 Elbow, 90 Degree, Variable Inlet/Outlet Areas, Supply Air Systems**

$H/W_1$	$C_o$ Values						
	0.6	0.8	1.0	$W_o/W_1$			
				1.2	1.4	1.6	2.0
0.25	0.63	0.92	1.24	1.64	2.14	2.71	4.24
1.00	0.61	0.87	1.15	1.47	1.86	2.30	3.36
4.00	0.53	0.70	0.90	1.17	1.49	1.84	2.64
100.	0.54	0.67	0.79	0.99	1.23	1.54	2.20



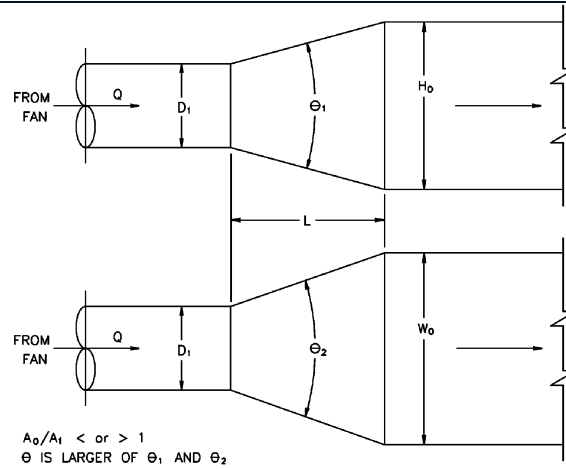
**SR4-1 Transition, Rectangular, Two Sides Parallel, Symmetrical, Supply Air Systems**



$A_o/A_1 < \text{or} > 1$

$A_o/A_1$	$C_o$ Values												
	$\theta$												
	0	3	5	10	15	20	30	45	60	90	120	150	180
0.10	0.0	0.12	0.09	0.05	0.05	0.05	0.05	0.06	0.08	0.19	0.29	0.37	0.43
0.167	0.0	0.11	0.09	0.05	0.04	0.04	0.04	0.06	0.07	0.19	0.28	0.36	0.42
0.25	0.0	0.10	0.08	0.05	0.04	0.04	0.04	0.06	0.07	0.18	0.27	0.36	0.41
0.50	0.0	0.08	0.09	0.06	0.04	0.04	0.04	0.06	0.07	0.12	0.17	0.20	0.27
1.00	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.00
2.00	0.0	0.64	0.96	0.54	0.52	0.62	0.94	1.40	1.48	1.52	1.48	1.44	1.40
4.00	0.0	4.16	4.64	2.72	3.09	4.00	6.72	9.60	10.88	11.20	11.20	10.88	10.56
6.00	0.0	12.24	10.08	7.38	8.10	10.80	17.28	23.40	27.36	29.88	29.88	29.34	28.80
10.00	0.0	40.50	27.20	23.30	25.10	34.00	52.84	69.00	82.50	93.50	93.50	92.40	91.30
16.00	0.0	112.64	68.35	63.74	67.84	92.93	142.13	182.53	220.16	254.21	254.21	251.90	249.60

SR4-3 Transition, Round to Rectangular, Supply Air Systems



C<sub>o</sub> Values

A <sub>o</sub> /A <sub>1</sub>	θ												
	0	3	5	10	15	20	30	45	60	90	120	150	180
0.10	0.0	0.12	0.09	0.05	0.05	0.05	0.05	0.06	0.08	0.19	0.29	0.37	0.43
0.167	0.0	0.11	0.08	0.05	0.05	0.05	0.05	0.06	0.07	0.19	0.28	0.37	0.42
0.25	0.0	0.10	0.07	0.05	0.05	0.05	0.05	0.06	0.07	0.17	0.27	0.35	0.41
0.50	0.0	0.08	0.07	0.06	0.07	0.06	0.05	0.06	0.07	0.13	0.19	0.23	0.24
1.00	0.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2.00	0.0	0.57	0.55	0.61	0.87	1.00	1.20	1.30	1.30	1.30	1.28	1.24	1.20
4.00	0.0	2.60	2.84	3.92	5.72	7.20	8.32	9.28	9.92	10.24	10.24	10.24	10.24
6.00	0.0	6.57	6.75	10.62	15.84	18.90	22.50	25.74	27.90	28.44	28.44	28.35	28.26
10.00	0.0	17.25	18.75	30.00	45.00	53.00	63.50	75.00	84.0	89.00	89.00	88.50	88.00
16.00	0.0	42.75	48.13	77.57	116.74	136.45	164.10	196.86	224.26	241.92	241.92	240.38	238.59

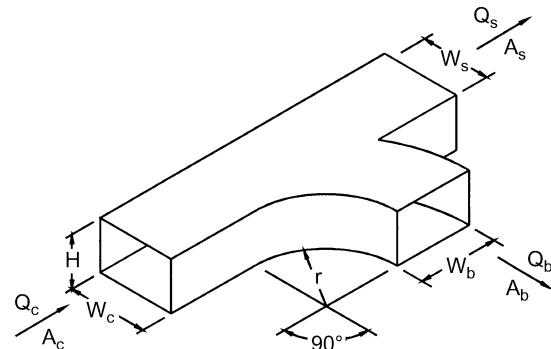
SR5-1 Smooth Wye of Type A<sub>s</sub> + A<sub>b</sub> ≥ A<sub>c</sub>, Branch 90° to Main, Diverging

C<sub>b</sub> Values

A <sub>s</sub> /A <sub>c</sub>	A <sub>b</sub> /A <sub>c</sub>	Q <sub>b</sub> /Q <sub>c</sub>								
		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.50	0.25	2.25	0.48	0.25	0.18	0.17	0.16	0.17	0.17	0.17
	0.50	11.00	2.38	1.06	0.64	0.52	0.47	0.47	0.47	0.48
	1.00	60.00	13.00	4.78	2.06	0.96	0.47	0.31	0.27	0.26
0.75	0.25	2.19	0.55	0.35	0.31	0.33	0.35	0.36	0.37	0.39
	0.50	13.00	2.50	0.89	0.47	0.34	0.31	0.32	0.36	0.43
	1.00	70.00	15.00	5.67	2.63	1.36	0.78	0.53	0.41	0.36
1.00	0.25	3.44	0.78	0.42	0.33	0.30	0.31	0.40	0.42	0.46
	0.50	15.50	3.00	1.11	0.63	0.48	0.42	0.40	0.42	0.46
	1.00	67.00	13.75	5.11	2.31	1.28	0.81	0.59	0.47	0.46

C<sub>s</sub> Values

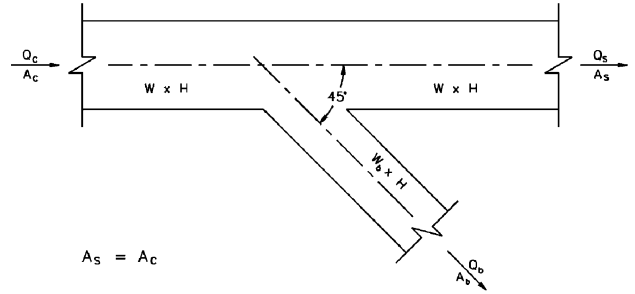
A <sub>s</sub> /A <sub>c</sub>	A <sub>b</sub> /A <sub>c</sub>	Q <sub>s</sub> /Q <sub>c</sub>								
		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.50	0.25	8.65	1.12	0.21	0.05	0.06	0.10	0.15	0.19	0.24
	0.50	7.50	0.98	0.19	0.06	0.06	0.10	0.14	0.18	0.22
	1.00	5.21	0.68	0.15	0.06	0.07	0.10	0.13	0.16	0.19
0.75	0.25	19.62	3.25	0.86	0.23	0.05	0.02	0.00	0.00	0.05
	0.50	20.62	3.24	0.76	0.14	-0.03	-0.07	-0.05	-0.01	0.03
	1.00	17.01	2.55	0.55	0.07	-0.05	-0.05	-0.02	0.02	0.06
1.00	0.25	46.00	9.50	3.22	1.31	0.52	0.14	-0.02	-0.05	-0.01
	0.50	35.34	6.49	1.98	0.69	0.22	0.00	-0.04	-0.05	-0.05
	1.00	38.95	7.10	2.15	0.74	0.23	0.03	-0.04	-0.05	-0.04



A<sub>s</sub> = A<sub>b</sub> ≥ A<sub>c</sub>  
r/W<sub>b</sub> = 1.0

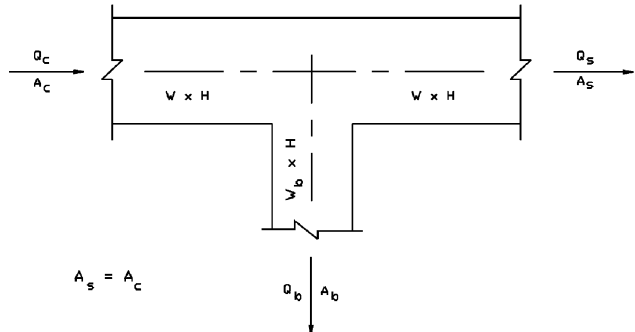
**SR5-3 Wye of the Type  $A_s + A_b > A_c, A_s = A_c, 45$  Degree, Diverging**

		$C_b$ Values								
		$Q_b/Q_c$								
$A_b/A_c$		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1		0.60	0.52	0.57	0.58	0.64	0.67	0.70	0.71	0.73
0.2		2.24	0.56	0.44	0.45	0.51	0.54	0.58	0.60	0.62
0.3		5.93	1.08	0.52	0.41	0.43	0.46	0.49	0.52	0.54
0.4		10.61	1.89	0.72	0.43	0.34	0.31	0.31	0.33	0.34
0.5		17.70	3.23	1.14	0.59	0.40	0.31	0.30	0.30	0.31
0.6		26.66	5.01	1.75	0.84	0.50	0.36	0.31	0.30	0.30
0.7		37.49	7.22	2.53	1.17	0.66	0.43	0.35	0.32	0.30
0.8		50.20	9.87	3.49	1.61	0.88	0.54	0.41	0.35	0.32
0.9		64.77	12.95	4.63	2.13	1.14	0.69	0.50	0.40	0.35
$Q_s/Q_c$		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
$C_s$		32.40	6.40	2.18	0.90	0.40	0.18	0.07	0.03	0.00



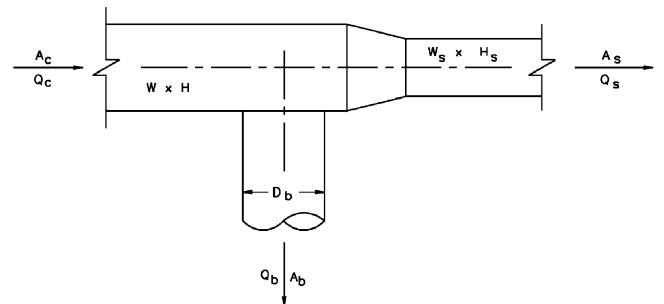
**SR5-5 Tee of the Type  $A_s + A_b > A_c, A_s = A_c$ , Diverging**

		$C_b$ Values								
		$Q_b/Q_c$								
$A_b/A_c$		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1		2.06	1.20	0.99	0.87	0.88	0.87	0.87	0.86	0.86
0.2		5.15	1.92	1.29	1.03	0.99	0.94	0.92	0.90	0.89
0.3		10.30	3.12	1.78	1.28	1.16	1.06	1.01	0.97	0.94
0.4		15.90	4.35	2.24	1.48	1.11	0.88	0.80	0.75	0.72
0.5		24.31	6.31	3.04	1.90	1.35	1.03	0.91	0.83	0.78
0.6		34.60	8.70	4.03	2.41	1.65	1.22	1.04	0.94	0.87
0.7		46.75	11.53	5.19	3.01	2.00	1.44	1.20	1.06	0.96
0.8		60.78	14.79	6.53	3.70	2.40	1.69	1.38	1.20	1.07
0.9		76.67	18.49	8.05	4.49	2.86	1.98	1.59	1.36	1.20
$Q_s/Q_c$		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	1.0
$C_s$		32.40	6.40	2.18	0.90	0.40	0.18	0.07	0.03	0.00



**SR5-11 Tee, Rectangular Main to Round Tap, Diverging**

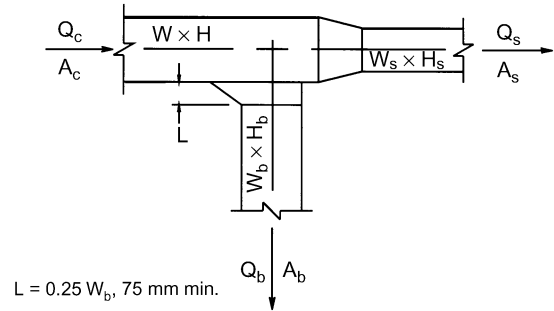
		$C_b$ Values								
		$Q_b/Q_c$								
$A_b/A_c$		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1		1.58	0.94	0.83	0.79	0.77	0.76	0.76	0.76	0.75
0.2		4.20	1.58	1.10	0.94	0.87	0.83	0.80	0.79	0.78
0.3		8.63	2.67	1.58	1.20	1.03	0.91	0.88	0.85	0.83
0.4		14.85	4.20	2.25	1.58	1.27	1.10	1.00	0.94	0.90
0.5		22.87	6.19	3.13	2.07	1.58	1.32	1.16	1.06	0.99
0.6		32.68	8.63	4.20	2.67	1.96	1.58	1.35	1.20	1.10
0.7		44.30	11.51	5.48	3.38	2.41	1.89	1.58	1.38	1.24
0.8		57.71	14.85	6.95	4.20	2.94	2.25	1.84	1.58	1.40
0.9		72.92	18.63	8.63	5.14	3.53	2.67	2.14	1.81	1.58
		$C_s$ Values								
		$Q_s/Q_c$								
$A_s/A_c$		0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1		0.04	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.2		0.98	0.04	0.01	0.00	0.00	0.00	0.00	0.00	0.00
0.3		3.48	0.31	0.04	0.01	0.00	0.00	0.00	0.00	0.00
0.4		7.55	0.98	0.18	0.04	0.02	0.00	0.00	0.00	0.00
0.5		13.18	2.03	0.49	0.13	0.04	0.00	0.01	0.00	0.00
0.6		20.38	3.48	0.98	0.31	0.10	0.04	0.02	0.01	0.00
0.7		29.15	5.32	1.64	0.60	0.23	0.09	0.04	0.02	0.01
0.8		39.48	7.55	2.47	0.98	0.42	0.18	0.08	0.04	0.02
0.9		51.37	10.17	3.48	1.46	0.67	0.31	0.15	0.07	0.04



**SR5-13 Tee, 45 Degree Entry Branch, Diverging**

<i>C<sub>b</sub> Values</i>									
<i>Q<sub>b</sub>/Q<sub>c</sub></i>									
<i>A<sub>b</sub>/A<sub>c</sub></i>	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1	0.32	0.33	0.32	0.34	0.32	0.37	0.38	0.39	0.40
0.2	0.31	0.32	0.41	0.34	0.32	0.32	0.33	0.34	0.35
0.3	1.86	1.65	0.73	0.47	0.37	0.34	0.32	0.32	0.32
0.4	3.56	3.10	1.28	0.73	0.51	0.41	0.36	0.34	0.32
0.5	5.74	4.93	2.07	1.12	0.73	0.54	0.44	0.38	0.35
0.6	8.48	7.24	3.10	1.65	1.03	0.73	0.56	0.47	0.41
0.7	11.75	10.00	4.32	3.31	1.42	0.98	0.73	0.58	0.49
0.8	15.57	13.22	5.74	3.10	1.90	1.28	0.94	0.73	0.60
0.9	19.92	16.90	7.38	4.02	2.46	1.65	1.19	0.91	0.73

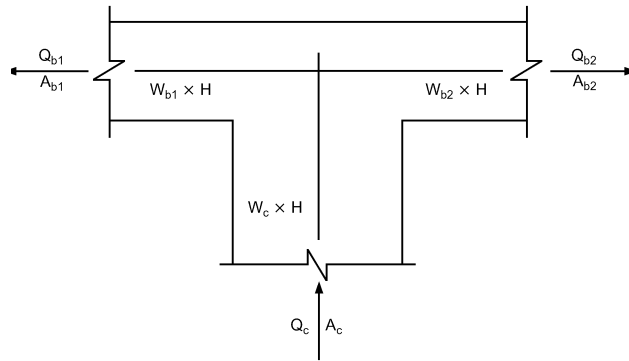
<i>C<sub>s</sub> Values</i>									
<i>Q<sub>s</sub>/Q<sub>c</sub></i>									
<i>A<sub>s</sub>/A<sub>c</sub></i>	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1	0.04	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.2	0.98	0.04	0.01	0.00	0.00	0.00	0.00	0.00	0.00
0.3	3.48	0.31	0.04	0.01	0.00	0.00	0.00	0.00	0.00
0.4	7.55	0.98	0.18	0.04	0.02	0.00	0.00	0.00	0.00
0.5	13.18	2.03	0.49	0.13	0.04	0.00	0.01	0.00	0.00
0.6	20.38	3.48	0.98	0.31	0.10	0.04	0.02	0.01	0.00
0.7	29.15	5.32	1.64	0.60	0.23	0.09	0.04	0.02	0.01
0.8	39.48	7.55	2.47	0.98	0.42	0.18	0.08	0.04	0.02
0.9	51.37	10.17	3.48	1.46	0.67	0.31	0.15	0.07	0.04



**SR5-15 Bullhead Tee Without Vanes, Diverging**

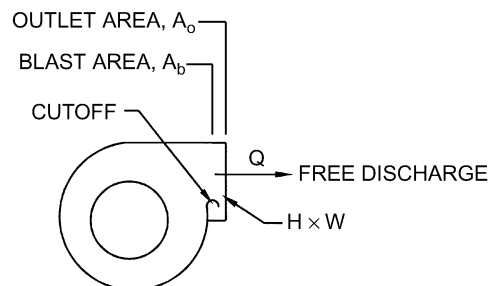
<i>C<sub>b1</sub> Values</i>									
<i>Q<sub>b1</sub>/Q<sub>c</sub></i>									
<i>A<sub>b1</sub>/A<sub>c</sub></i>	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.1	1.34	0.53	0.37	0.30	0.29	0.28	0.27	0.27	0.27
0.2	4.43	1.25	0.66	0.45	0.39	0.35	0.32	0.31	0.30
0.3	9.58	2.45	1.16	0.71	0.56	0.47	0.41	0.37	0.35
0.4	16.87	4.17	1.88	1.09	0.73	0.53	0.38	0.33	0.30
0.5	26.19	6.35	2.79	1.56	1.01	0.71	0.49	0.41	0.37
0.6	37.57	9.02	3.89	2.14	1.35	0.92	0.62	0.52	0.45
0.7	51.03	12.17	5.20	2.82	1.75	1.18	0.78	0.64	0.54
0.8	66.55	15.81	6.71	3.61	2.22	1.48	0.96	0.78	0.65
0.9	84.15	19.93	8.42	4.50	2.74	1.81	1.17	0.94	0.78

For other branch, subscripts 1 and 2 change places.



**SR7-1 Fan, Centrifugal, Without Outlet Diffuser, Free Discharge**

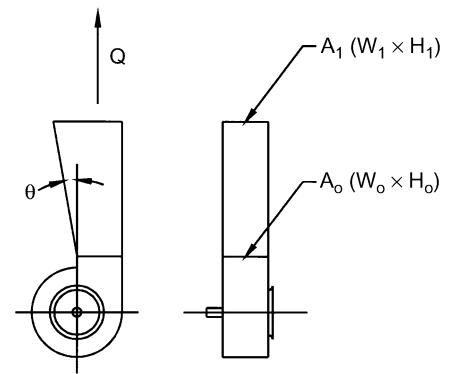
<i>A<sub>b</sub>/A<sub>o</sub></i>	0.4	0.5	0.6	0.7	0.8	0.9	1.0
<i>C<sub>o</sub></i>	2.00	2.00	1.00	0.80	0.47	0.22	0.00



**SR7-2 Plane Asymmetric Diffuser at Centrifugal Fan Outlet, Free Discharge**

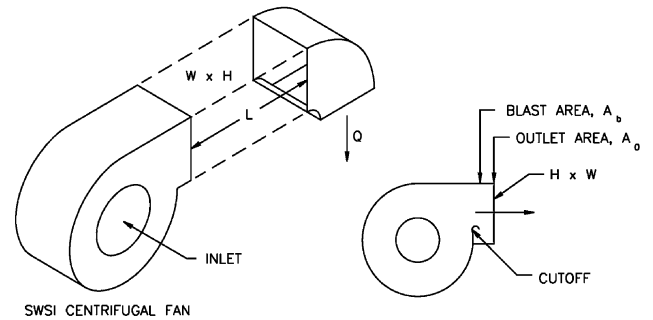
$\theta$	$C_o$ Values					
	$A_1/A_o$					
	1.5	2.0	2.5	3.0	3.5	4.0
10	0.51	0.34	0.25	0.21	0.18	0.17
15	0.54	0.36	0.27	0.24	0.22	0.20
20	0.55	0.38	0.31	0.27	0.25	0.24
25	0.59	0.43	0.37	0.35	0.33	0.33
30	0.63	0.50	0.46	0.44	0.43	0.42
35	0.65	0.56	0.53	0.52	0.51	0.50

FREE DISCHARGE



**SR7-5 Fan Outlet, Centrifugal, SWSI, with Elbow (Position A)**

$A_b/A_o$	$C_o$ Values					
	$L/L_e$					
	0.00	0.12	0.25	0.50	1.0	10.0
0.4	3.20	2.50	1.80	0.80	0.0	0.0
0.5	2.20	1.80	1.20	0.53	0.0	0.0
0.6	1.60	1.40	0.80	0.40	0.0	0.0
0.7	1.00	0.80	0.53	0.26	0.0	0.0
0.8	0.80	0.67	0.47	0.18	0.0	0.0
0.9	0.53	0.47	0.33	0.18	0.0	0.0
1.0	0.53	0.47	0.33	0.18	0.0	0.0



$$V_o > 13 \text{ m/s: } L_e = \frac{V_o \sqrt{A_o}}{4500}$$

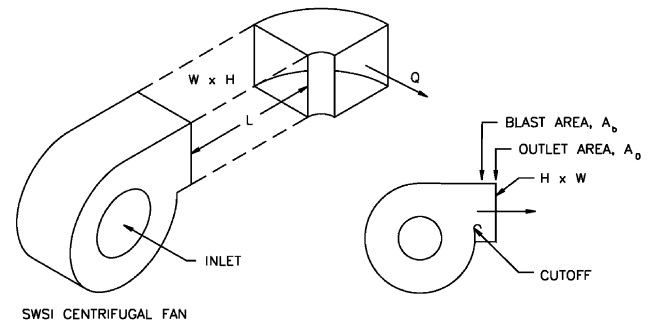
$$V_o \leq 13 \text{ m/s: } L_e = \frac{\sqrt{A_o}}{350}$$

where:

- $V_o$  = duct velocity, m/s
- $L_e$  = effective duct length, m
- $A_o$  = duct area, mm<sup>2</sup>

**SR7-6 Fan Outlet, Centrifugal, SWSI, with Elbow (Position B)**

$A_b/A_o$	$C_o$ Values					
	$L/L_e$					
	0.00	0.12	0.25	0.50	1.0	10.0
0.4	3.80	3.20	2.20	1.00	0.0	0.0
0.5	2.90	2.20	1.60	0.67	0.0	0.0
0.6	2.00	1.60	1.20	0.53	0.0	0.0
0.7	1.40	1.00	0.67	0.33	0.0	0.0
0.8	1.00	0.80	0.53	0.26	0.0	0.0
0.9	0.80	0.67	0.47	0.18	0.0	0.0
1.0	0.67	0.53	0.40	0.18	0.0	0.0

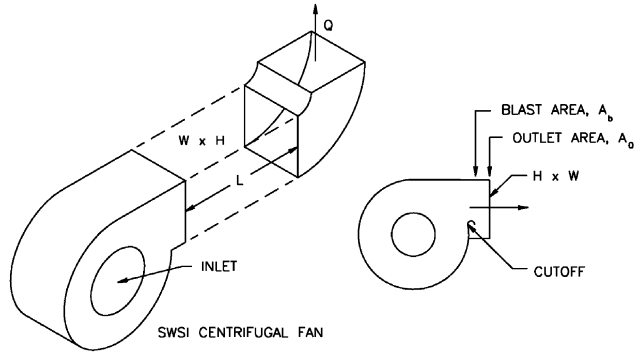


To calculate  $L_e$ , see Fitting SR7-5.



**SR7-7 Fan Outlet, Centrifugal, SWSI, with Elbow (Position C)**

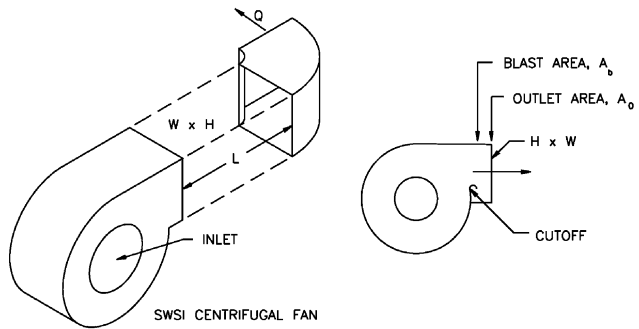
$A_b/A_o$	$C_o$ Values					
	$L/L_e$					
	0.00	0.12	0.25	0.50	1.0	10.0
0.4	5.50	4.50	3.20	1.60	0.0	0.0
0.5	3.80	3.20	2.20	1.00	0.0	0.0
0.6	2.90	2.50	1.60	0.80	0.0	0.0
0.7	2.00	1.60	1.00	0.53	0.0	0.0
0.8	1.40	1.20	0.80	0.33	0.0	0.0
0.9	1.20	0.80	0.67	0.26	0.0	0.0
1.0	1.00	0.80	0.53	0.26	0.0	0.0



To calculate  $L_e$ , see Fitting SR7-5.

**SR7-8 Fan Outlet, Centrifugal, SWSI, with Elbow (Position D)**

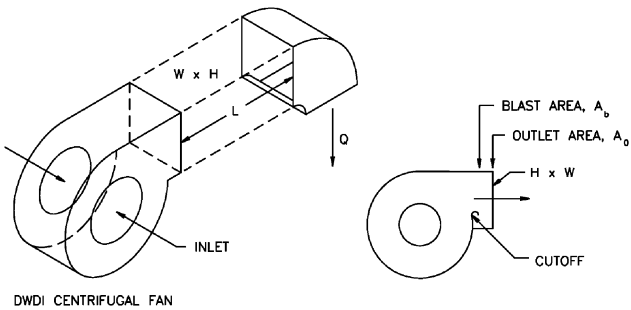
$A_b/A_o$	$C_o$ Values					
	$L/L_e$					
	0.00	0.12	0.25	0.50	1.0	10.0
0.4	5.50	4.50	3.20	1.60	0.0	0.0
0.5	3.80	3.20	2.20	1.00	0.0	0.0
0.6	2.90	2.50	1.60	0.80	0.0	0.0
0.7	2.00	1.60	1.00	0.53	0.0	0.0
0.8	1.40	1.20	0.80	0.33	0.0	0.0
0.9	1.20	0.80	0.67	0.26	0.0	0.0
1.0	1.00	0.80	0.53	0.26	0.0	0.0



To calculate  $L_e$ , see Fitting SR7-5.

**SR7-9 Fan Outlet, Centrifugal, DWDI, with Elbow (Position A)**

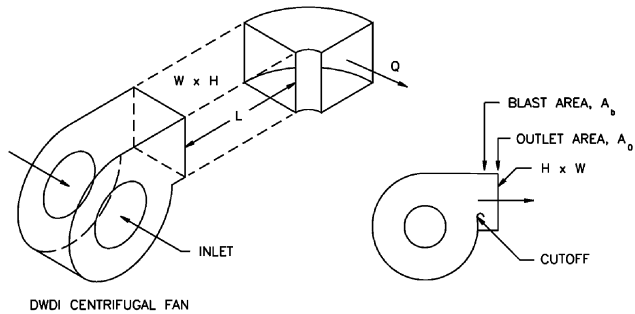
$A_b/A_o$	$C_o$ Values					
	$L/L_e$					
	0.00	0.12	0.25	0.50	1.0	10.0
0.4	3.20	2.50	1.80	0.80	0.0	0.0
0.5	2.20	1.80	1.20	0.53	0.0	0.0
0.6	1.60	1.40	0.80	0.40	0.0	0.0
0.7	1.00	0.80	0.53	0.26	0.0	0.0
0.8	0.80	0.67	0.47	0.18	0.0	0.0
0.9	0.53	0.47	0.33	0.18	0.0	0.0
1.0	0.53	0.47	0.33	0.18	0.0	0.0



To calculate  $L_e$ , see Fitting SR7-5.

**SR7-10 Fan Outlet, Centrifugal, DWDI, with Elbow (Position B)**

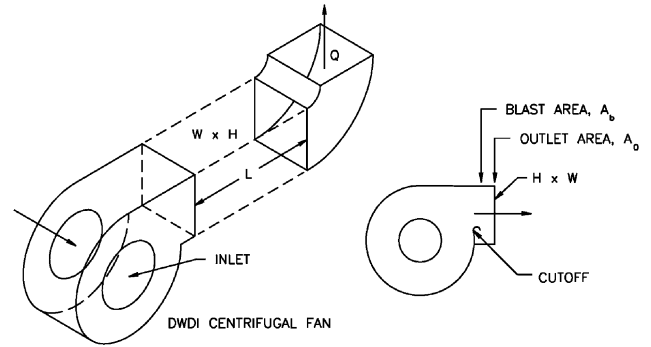
$A_b/A_o$	$C_o$ Values					
	$L/L_e$					
	0.00	0.12	0.25	0.50	1.0	10.0
0.4	4.80	4.00	2.90	1.30	0.0	0.0
0.5	3.60	2.90	2.00	0.84	0.0	0.0
0.6	2.50	2.00	1.50	0.66	0.0	0.0
0.7	1.80	1.30	0.84	0.41	0.0	0.0
0.8	1.25	1.00	0.66	0.33	0.0	0.0
0.9	1.00	0.84	0.59	0.23	0.0	0.0
1.0	0.84	0.66	0.50	0.23	0.0	0.0



To calculate  $L_e$ , see Fitting SR7-5.

**SR7-11 Fan Outlet, Centrifugal, DWDI, with Elbow (Position C)**

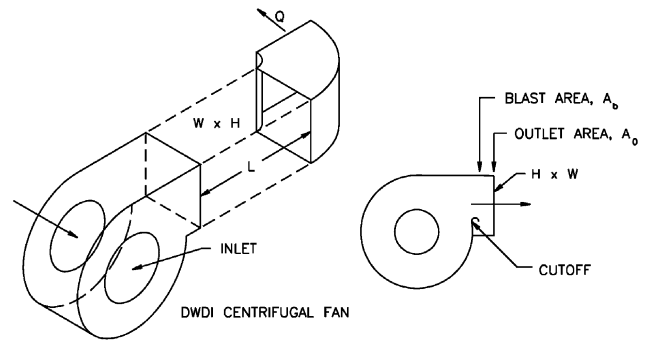
$A_b/A_o$	$C_o$ Values					
	$L/L_e$					
	0.00	0.12	0.25	0.50	1.0	10.0
0.4	5.50	4.50	3.20	1.60	0.0	0.0
0.5	3.80	3.20	2.20	1.00	0.0	0.0
0.6	2.90	2.50	1.60	0.80	0.0	0.0
0.7	2.00	1.60	1.00	0.53	0.0	0.0
0.8	1.40	1.20	0.80	0.33	0.0	0.0
0.9	1.20	0.80	0.67	0.26	0.0	0.0
1.0	1.00	0.80	0.53	0.26	0.0	0.0



To calculate  $L_e$ , see Fitting SR7-5.

**SR7-12 Fan Outlet, Centrifugal, DWDI, with Elbow (Position D)**

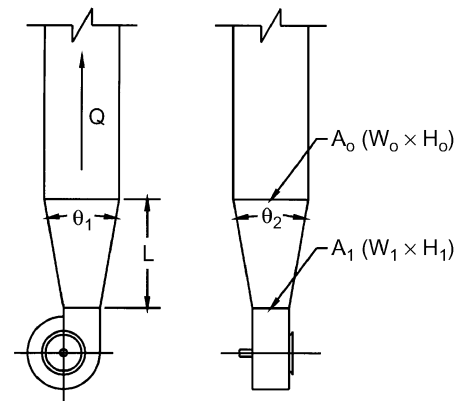
$A_b/A_o$	$C_o$ Values					
	$L/L_e$					
	0.00	0.12	0.25	0.50	1.0	10.0
0.4	4.70	3.80	2.70	1.40	0.0	0.0
0.5	3.20	2.70	1.90	0.85	0.0	0.0
0.6	2.50	2.10	1.40	0.68	0.0	0.0
0.7	1.70	1.40	0.85	0.45	0.0	0.0
0.8	1.20	1.00	0.68	0.26	0.0	0.0
0.9	1.00	0.68	0.57	0.22	0.0	0.0
1.0	0.85	0.68	0.45	0.22	0.0	0.0



To calculate  $L_e$ , see Fitting SR7-5.

**SR7-17 Pyramidal Diffuser at Centrifugal Fan Outlet with Ductwork**

$\theta$	$C_1$ Values						
	$A_o/A_1$						
	1.0	1.5	2.0	2.5	3.0	3.5	4.0
0	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10	0.00	0.10	0.18	0.21	0.23	0.24	0.25
15	0.00	0.23	0.33	0.38	0.40	0.42	0.44
20	0.00	0.31	0.43	0.48	0.53	0.56	0.58
25	0.00	0.36	0.49	0.55	0.58	0.62	0.64
30	0.00	0.42	0.53	0.59	0.64	0.67	0.69



$\theta$  is larger of  $\theta_1$  and  $\theta_2$

$$C_o = C_1 \left( \frac{A_o}{A_1} \right)^2$$